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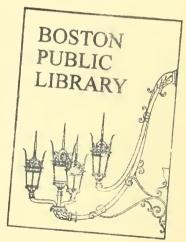
## HYNES AUDITORIUM EXPANSION BOSTON, MASSACHUSETTS

## Final Report (Volume II – Part C)

### Support Documentation

Code/Fire Protection
Heating Ventilating & Air Conditioning

Plumbing Electrical



CITY OF BOSTON Kevin H. White, Mayor

BOSTON REDEVELOPMENT AUTHORITY Robert J. Ryan, Director

PUBLIC FACILITIES DEPARTMENT Donald B. Manson, Director





# Final Report (Volume II - Part C) Support Documentation

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Code/Fire Protection
Heating Ventilating & Air Conditioning
Plumbing
Electrical



#### INTRODUCTION

The back-up data provided in this volume was used by the consultants in the design process for the Hynes Auditorium Expansion and serves as technical support for the contents of the consultants' reports in Volume I/Architectural and Engineering Summary portion of the Final Report.





Code/Fire Protection



#### INDEX

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Fire Detection and Alarm System
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Smoke Control Systems

FIREPRO File: 6K1202

#### EXISTING CONDITIONS

#### Analysis of Means of Egress

An approximate analysis of the relation between building population and exit capacity indicates three significant problems exist with respect to the means of egress system.

The anticipated population of the Second Level exhibit and meeting room spaces exceeds the capacity available in enclosed exit stairs, unenclosed monumental stairs and doors into the Sheraton Boston.

On the Main Level, the anticipated population does not exceed the exit capacity available on that floor. However, the number of persons from the Second Level who will use open stairs to the Main Level must be added to the Main Level population. This total population of persons using Main Level doors to the outside does exceed the capacity of the doors available.

The distribution of exits on the Main Level does not match the population distribution. Specifically, a high percentage of the exit capacity available is concentrated at the main entrance/exit lobby at the corner of Boylston and Dalton Streets while the building population will be relatively uniformly distributed throughout the building.



#### CONCEPTUAL FIRE DEFENSE PROGRAM Option IV A

The fire defense features of the expanded and renovated Hynes Auditorium will be required to comply with the Massachusetts State Building Code (MSBC), 4th Edition. Article 22 of the MSBC concerning the renovation and expansion of the existing building provides general requirements applicable to this project. Sections 2200.0, 2201.0, 2202.0 and 2203.0 are the specifically applicable sections of this Article which affect the Hynes Auditorium project.

For all practical purposes, these sections require that both the new and existing portions of the facility must comply with the requirements of the main body of the Building Code for new construction. As further details of the renovation work are developed, it may be that portions of Article 22 will allow relaxation of the strict requirements for new construction in the areas of the existing facility being renovated. No attempt has been conducted to date to identify such specific details for the portions of the facility being renovated.

The following discussion identifies the primary requirements of the MSBC which will impact upon this building.

#### Structural Fire Resistance

The existing Hynes Auditorium is of fire resistive construction, construction Type 1A as described in the MSBC, Table 214. Strict height and area limitations of the Building Code as documented in Table 305 and Exceptions to that Table would require the building to be of Type 1A or 1B construction. It is anticipated Type 1A construction will be utilized to match the construction classification of the existing portions of the facility.

#### Barriers to Vertical Fire Spread

The floor assembly will have a fire rating of 3 hours in accordance with the requirements for Type IA construction. Shafts penetrating these floor systems for enclosed stairs and for mechanical and electrical systems will have a 2 hour fire rating.

The facility will be arranged in accordance with Article 437.0, Open Wells, including subsections 437.2 concerning atriums and Section 616.8, Supplemental Stairs, to permit the multiple levels of the facility to be interconnected. The atrium requirements will be applied to the Grand Lobby, East Lobby and



South Lobby areas. The supplemental stairs section will be applied to the escalators between exhibition spaces on the Main Level and the Second Level.

#### Barriers to Horizontal Fire Spread

Two hour fire partitions will be provided which separate the Second Level auditorium from the adjacent Second Level exhibition space and the Third Level portions of the auditorium from the Third Level conference/exhibition space.

One hour fire rated partitions will be used to separate meeting rooms from adjacent prefunction areas serving as exit access corridors.

One hour fire rated partitions or smoke stop partitions which may include plain glass will be used to separate the exhibition and meeting spaces of the Lower Level, Main Level, Second Level and Third Level from the lobbies of the building arranged as atriums.

Figures No. 1 through 5 illustrate the location of fire rated or smoke stop partitions.

#### Fire Detection and Alarm System

A new fire detection and alarm system will be provided for the facility. Conceptually, this system will be subdivided into zones on a floor by floor basis and into additional zones related to the three lobbies and other major functional areas. Table No. 1 provides a general listing of the primary fire alarm system zones. Figures No. 7 through 11 illustrate the arrangement of these zones.

Within each zone, additional distinct zones will be provided for automatic fire detectors other than waterflow detectors (smoke detectors, heat detectors), waterflow detectors and manual pull stations.

Alarms from automatic or manual fire detection devices will be used to initiate a variety of building system reaction including transmission of fire alarms to the Boston Fire Department, activation of evacuation signals in the entire building. Other building system reactions may include release of hold-open devices for doors in fire rated and smoke stop partitions, activation of smoke control systems, shut down of affected HVAC systems, and start-up of the fire pump of the automatic sprinkler and standpipe and water supply systems.

Figure No. 6 is a matrix which documents the types of detection devices provided and the primary building system reactions upon alarm of those detection devices.



The fire alarm system will also be utilized to provide supervisory functions for primary elements of the fire protection systems of the building. These elements are also listed in Figure No. 6.

In addition to these automatic functions of the fire alarm system, manual controls for use by the Boston Fire Department will be provided for the fire alarm system, elevators, smoke control equipment and some other elements of the fire protection system.

#### Means of Egress

The means of egress system for the Hynes Auditorium is based upon a number of enclosed interior stairs leading to discharge through lobbies, exit discharge passageways or directly to the exterior at various levels of the building. This is a result of the change in grade of the site around the building. In addition, because multiple levels have access to the exterior, doors directly to the exterior are provided on several levels.

Limited use of horizontal exits into the Sheraton Boston Hotel is anticipated by this exiting scheme.

Horizontal exits may also be developed within the facility on the Second and Third Levels. The effect of such internal horizontal exits is to subdivide the building population requiring immediate evacuation and to provide additional exit capacity without adding new stairs.

Tables 2, 3, 4 and 5 provide data to permit analysis of the balance of exit capacity against building population on a floor by floor basis. Basic information used in that analysis is indicated directly in Tables or as Notes to Tables.

This analysis indicates the need for more exit capacity than provided by the current design. When internal horizontal exits are provided, the balance of population and exit capacity on a fire area by fire area basis is acceptable for all areas except the third floor south conference/exhibition area. For the third floor south, the excess of population over exit capacity is approximately 800 persons. A combination of additional stair capacity, such as by providing access to Stair 12, plus additional horizontal exit capacity, should permit this problem to be resolved.

The exit discharge arrangements for the Hynes Auditorium and for the Sheraton Boston Hotel in the South Lobby-Retail area (also referred to as the West Court of the Prudential Plaza) have been reviewed. Although multiple paths from that area to grade are available, the capacity of those paths, as in the present



design, is not sufficient. Additional capacity may be develped by pulling the east end of the new retail space back to the line of the east side of Commercial Block A or widening the stairs which currently exist at the south end of the open space between the Sheraton Boston Hotel and Commercial Block A. Additional study to fully resolve these problems will be needed in the future design effort.

#### Automatic Sprinkler Systems

The facility will be provided with complete automatic sprinkler coverage using several automatic sprinkler systems with a common water supply and distribution system. The water supply system will also serve Fire Department hose connections on standpipes within stairwells.

Water will be supplied to the building from city mains on Boylston Street and Dalton Street. These connections will be manifolded together to supply a minimum of two electrically driven fire pumps. The fire pumps as well as a pump bypass will supply distribution piping to standpipes in enclosed exit stairs and at other locations as required for adequate coverage of the facility.

Automatic sprinkler systems will be connected to the standpipe risers and zoned as listed in Table No. 1 and as illustrated in Figures No. 7 through 11 for fire alarm system zones.

#### Smoke Control Systems

Exhaust fans will be provided at the highest levels of the Grand and East Lobbies to provide smoke exhaust capability in accordance with the atrium section of the MSBC. Other HVAC equipment may be used for smoke control purposes. Any equipment not so used will be automatically shut down to prevent recirculation of smoke which enters the HVAC system.

The South Lobby escalator will be equipped with an exhaust system which has intakes on each floor near the escalator opening. This system will be designed in accordance with the Massachusetts State Elevator Code.



#### TABLE NO. 1

## Primary Fire Alarm System Detection Zones

		TABLE NO. 1	tors
		Primary Fire Alarm System Detection Zones	SUBZONES Waterflow Smoke Detec Manual Pull
	Zone	Area	SU Wa Sm Ma
Third Level (See Figure No. 6)	3 - 1 3 - 2 3 - 3 3 - 4	Grand Lobby Conf./Exh./Mtg./Pref. East Lobby Mechanical	
Second Level (See Figure No. 7)	2-1 2-2 2-3 2-4 2-5 2-6 2-7	Grand Lobby Auditorium Boylston Street Mtg. Rooms Exhibition East Lobby East Meeting Rooms South Lobby/Meeting Rooms	
Main Level (See Figure No. 8)	M-1 M-2 M-3 M-4 M-5 M-6	Grand Lobby West Exhibition Central Exhibition/Pref. East Lobby East Meeting Rooms South Lobby	
Street Level (See Figure (No. 9)	S	East Lobby	• • •
Lower Level (See Figure No. 10)	L - 1 L - 2 L - 3	Meeting Rooms East Lobby Existing Loading Dock/Support	• • • • • • • • • • • • • • • • • • •



# TABLE NO. 2 Approximate Population Calculation Building Basis

	Du	Truing Busis	
Third Laval	Area (sf)	Density (sf/	p) Population (p)
Third Level Conf./Exhib. C/E Prefunction Meeting 3A Meeting 3B Meeting 3C Meeting 3D Prefunction East Lobby	35,250	7	5035
C/E Prefunction	7,320	-	-
Meeting 3A Meeting 3B	2,700	7 7	321 314
Meeting 3C	2,200	7	771
Meeting 3D	5,400	-	-
Prefunction East Lobby	8.248	-	-
Prefunction East Lobby Grand Lobby	10,300	<u>-</u>	-
TOTAL			6,441
Second Level Exhibition	52 096	15	3173
Auditorium	30,000	15 Anticipated Actual	Seating 4000
Audit. Balcony	6,512	7	930
Aud. Prefunction	11,400	15	760 -
Meeting 2A	7,448	7	1064
Meeting 2B	9,500	7	1357
Meeting 2C	3,364	, 7 7	487 746
Meeting 2E	3,364	7	487
Prefunction 2A/2B	9,360	, 7 - -	-
Prefunc. 2C/2D/2E	7,980		-
Auditorium Audit. Balcony Aud. Prefunction Grand Lobby Meeting 2A Meeting 2B Meeting 2C Meeting 2D Meeting 2E Prefunction 2A/2B Prefunc 2C/2D/2E East Lobby South Meeting South Lobby TOTAL	4,500	- 7	643
South Lobby	7,520	-	-
			13,017
Main Level East Exhibition	54,925	15	3662
West Exhibition	46,440	15	3096
Grand Lobby	6,624	-	- -
East Lobby	4.628	-	-
Meeting MA	5,568	7	795
Meeting MB	3,712	- - 7 7 7	530 414
West Exhibition Grand Lobby Prefunction East Lobby Meeting MA Meeting MB Meeting MC East Prefunction South Lobby	6.896	/ -	414
	3,960		-
TOTAL			8,497
Street Level Lobby	4,952	_	-
Lower Level	,,,,,,,		
Meeting LA	3,910	7 7	559
Meeting LB Meeting LC	3,840 2,640	7 7	406 377
Prefunction	8,008	-	-
Lobby	5,432	-	1 7/5
TOTAL			1,342

FIREPRO File: 6K1202

December 28, 1982



TABLE NO. 3

Available Exit Capacity
Building Basis

(Stair and Door Designations provided on Figures No. 1 to 5)

	Exit	uew	x	p/uew	=	Exit Capacity (p)
Third Level	S2	3	х	113	=	339
11110 20101	S3	3 3 5 3 3 3	X	113	=	339
	S5	5	X	113	=	565
	S7	3	X	113	=	339
	S8	3	x	113	=	339
	S9	3	X	113	=	339
	S10	6 5	X	113	=	678
	S11	5	X	113	=	565
	S13	4	X	113	=	452
	Total Ex	it Capa				3,955
Caran I I am I	6.2	7		117		770
Second Level	S2	3	X	113	=	339 339
	S3	<u>ي</u> د	X	113 113	=	565
	S5 S6	3	X	113	=	339
	S7	3	X X	113	=	339
	S8	7	X	113	~ =	339
	S9	3	X	113	=	339
	S10	6	X	113	=	678
	S11	5	x	113	=	565
	S12	3 5 3 3 3 6 5 4	x	113	=	452
	S13	4	X	113	=	452
	S14	6	X	113	=	678
	Subtotal					5,424
	D5	3	х	150	=	450
	D6	9	х	150	=	1,350
	D7	3	х	150	=	450
	Subtotal		apacit		Doors	2,250
	Total Ex	it Capac	ity			7,674



TABLE NO. 3 (cont'd)

	Exit	uew	х	p/uew	=	Exit Capacity (p)
Main Level	S2 S3 S6 S7 S8 S9 Subtota	3 3 3 3 3 3 L Exit	x x x x x x Capaci	113 113 113 113 113 113 ty For	= = = = = = Stairs	339 339 339 339 339 339 2,034
	D2 D3 D4 D8 D9 D10 Subtotal			150 150 150 150 150 150 150 ty For	= = = = = Stairs	2,250 1,350 1,800 450 450 450 6,750 8,784
Street Level	D1	36	х	150	=	5,400
Lower Level	S1 S2 S3 S4 Total Ex	3 2 3 3	x x x x x pacity	113 113 113 113	= = =	339 339 339 339 1,356



TABLE NO. 4 Approximate Population and Exit Capacity Calculations

#### Fire Area Basis

Second & Third Leve	Popula-	Exit Capacity Stair & Doors	Exit Capacity Internal Horizontal	Exit Capa-
Fire Area	tion	To Sheraton(p)	Exits(p)(5)	city(p)
Third Level South Conf./Exhibition	5035	21471	2147	4294
Third Level North C/E Prefunction Meeting Rooms Prefunction East Lobby Grand Lobby TOTAL	1406 - - - 1406	1808 <sup>2</sup>	1808	3616
Second Level East Exhibition Meeting Rooms Prefunction East Lobby South Lobby TOTAL	3473 4784 - - - 8257	4738 <sup>3</sup>	4738	9476
Second Level West Auditorium (incl. Balcony) Aud. Prefunction Grand Lobby TOTAL	4000 760 - 4760	2936 <sup>4</sup>	2936	5872
	. , 00	2330	2550	3012

- NOTES: (1) Stairs S7, S8, S9, S10, S13
  (2) Stairs S2, S3, S5, S11
  (3) Stairs S2, S3, S8, S9, S10, S12, S13/Doors D5, D6
  (4) Stairs S5, S6, S7, S11, S14/Door D7
  (5) Horizontal exit capacity for a specific fire area may not exceed the exit capacity available using other exit paths (stairs, doors to Sheraton).

Total



SUMMARY
Approximate Exit System Analysis

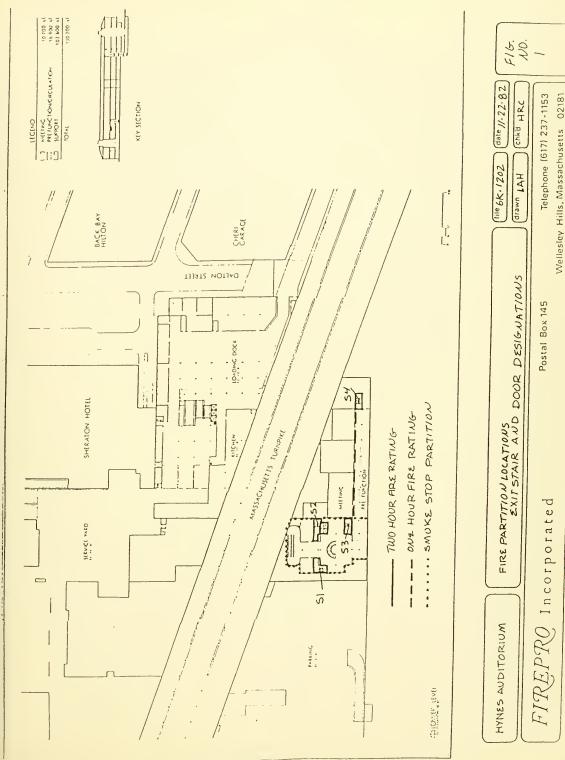
TABLE NO. 5

Level	Population	Option IV-A Floor By Floor Exit Capacity*	Option IV-A Fire Area by Fire Area Exit Capacity**
Third South North TOTAL	5,035 1,406 6,441	- - 3,955	4,294 3,616
Second East West TOTAL	8,725 4,760 13,017	- 7,674	9,476 5,872
Main	8,497	8,784	784
Lower	1,342	1,356	1,356

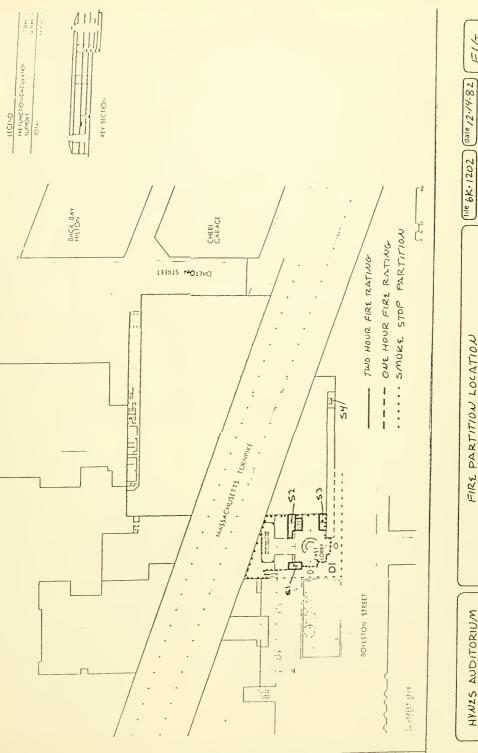
<sup>\*</sup> Based upon Option IV-A arrangement of stairway exits and horizontal exits into The Sheraton Boston Hotel.

<sup>\*\*</sup> Based upon subdivision of Levels Two and Three to allow use of internal horizontal exit concept.









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EXIT STAIR AND DOOR DESIGNATIONS

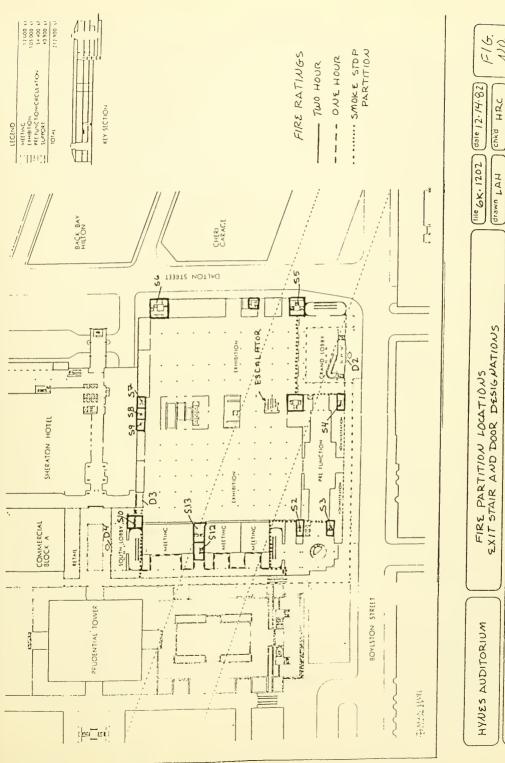
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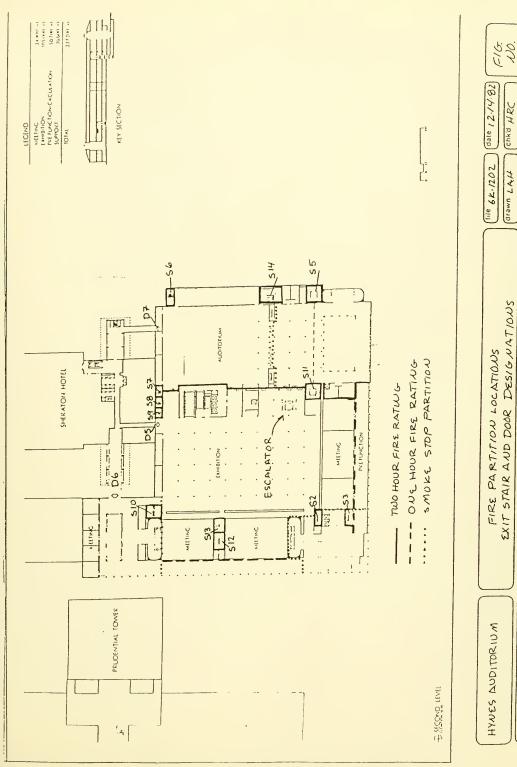
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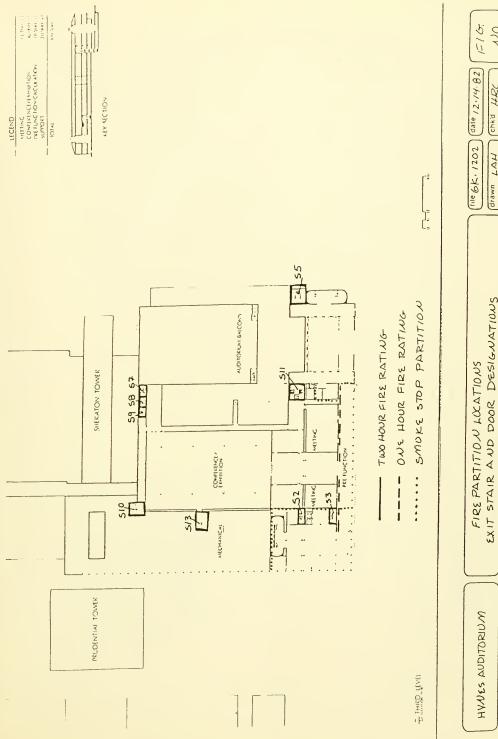




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	TRANSMITALARM TO B.F.D.	ANNUNCIATE ALARMS AT COUTROL PAUL	ANNUNCIATE DIARMS AT REMOTE ANNUNCIATOR (5)	RELEASS HOLD OPEN DOORS	ACTIVATE ALARM SIGNALS	RETURN ROOM WEHTS TO FULL BRIGHTNESS	ACTIVATE EXHAUST FAUS IN LOBBY OF A LARM ORIGIN.	SHUT DOWN HVAC SYSTEMS NOT USED FOR SMOKE CONTROL			REMOTE SIGNAL AT REMOTE AUDUNCIATOR	ANDUNCIATE SIGNAL ATCOUTROL PAUXL	
MANUAL PULL STATIONS	•	•	•	•	•	•		•					
SMOKE DETECTORS IN	•	•	•	•	•	•	•	•		 _			
LOBBY ZONES													
OTHER SMOKE DETECTORS	•	•	•	•	•	•		•					
(E (ELECTRICAL RAS ELU. RAS. ETC.)													]
HEAT DETECTORS (ELECTRICAL	•	•	•	•	•	•		•					
RMS, ELEVATOR RMS. ETC.)													
SPRINKLER WATERFLOW	•	•	•	•	•	•	•	•					
DETECTORS IN LOBBY ZONES													
OTHER SPRINKLER WATER-		•	•	•	•	•		•					
FLOW DETECTORS													
DUCT TYPE SMOKE DETECTORS	•	•	•					•		 			
		-			+	-	+	-	_				
			+				+						
SUPERVISORY/TROUBLE SIGUALS													
WATER SUPPLY SYSTEM											•	•	
VALVE TAMPER SWITCH													
LOW CITY WATER PRESSURE											•	•	
LOW SYSTEM WATER PRESURE											•	•	
FIRE PUMP POWER											•	•	
FIRE PUMP RUNNING									Ť		•	•	
EXHAUST FAN POWER											•	•	
EXHAUST FAN RUNNING											•	•	
CIRCUIT TROUBLE											•	•	

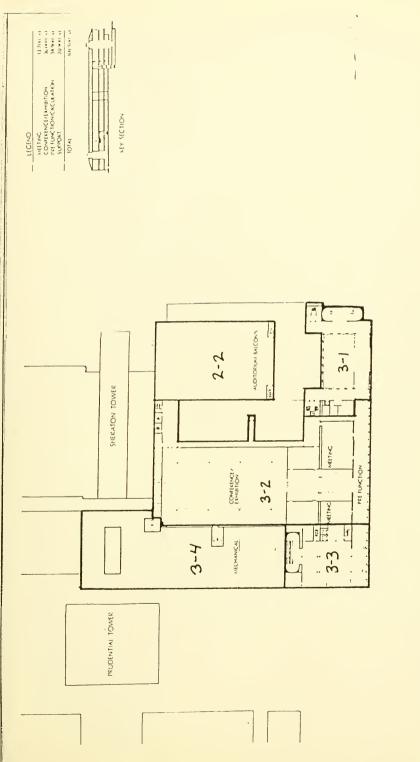
HYNES AUDITORIUM

BASIC FIRE ALARM SYSTEM OPERATIONS

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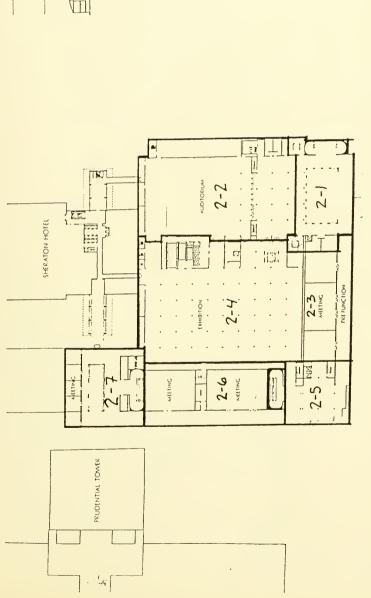
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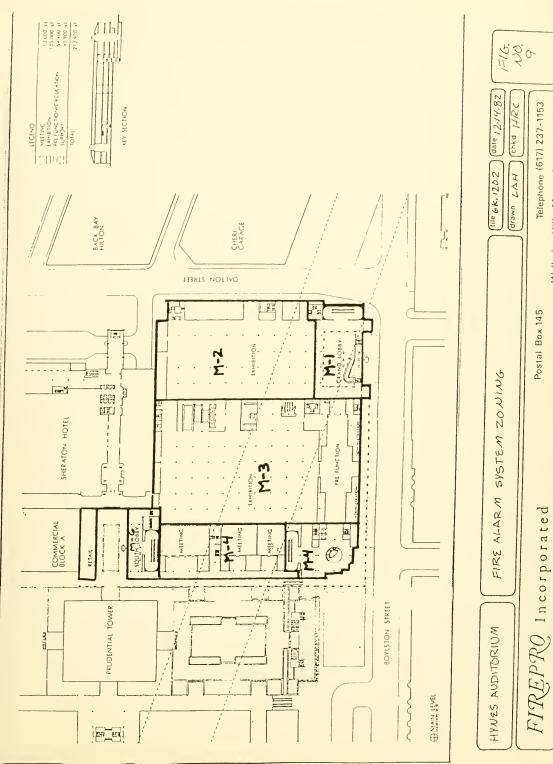
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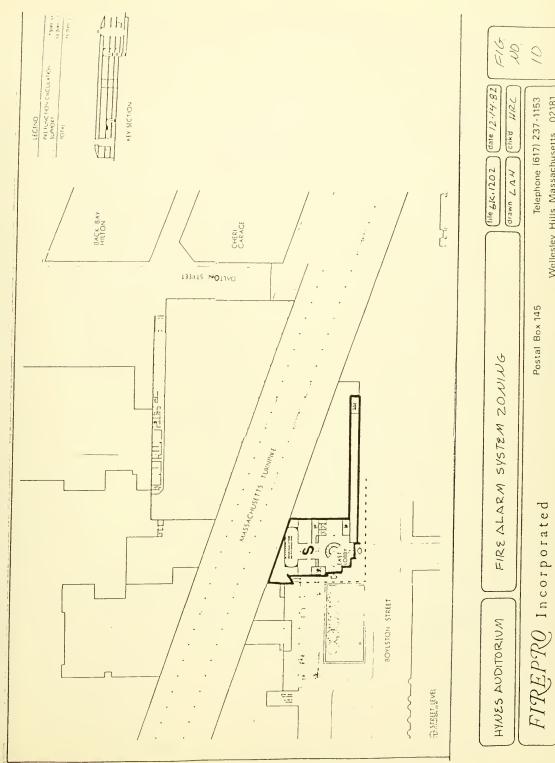
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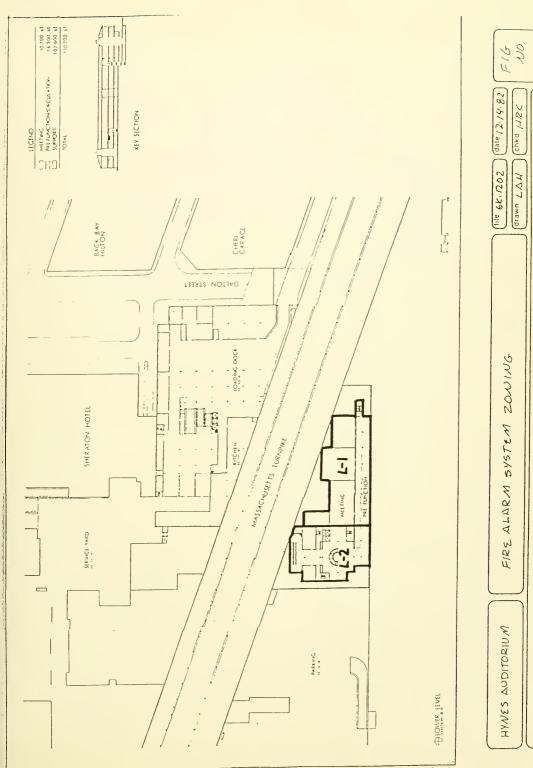










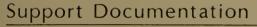


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Heating Ventilating & Air Conditioning



#### VI. SUPPORT DOCUMENTATION

TABLE 1: EXISTING STEAM CONNECTED HEATING LOADS.

TABLE 2: EXISTING PUMPS.

TABLE 3: AIR CONDITIONING UNITS.

TABLE 4: MAINTENANCE COSTS.

TABLE 5: UTILITY OPERATING COSTS.

TABLE 6: PRELIMINARY AIR HANDLING UNIT CAPACITY REQUIREMENTS.



TABLE 1: EXISTING CONNECTED STEAM HEATING LOADS

	ITEM/SERVICE	LOAD #/HR.	COMMENTS
1.	5 convertors - (steam to Hot Water	) 5740	See Note #1
2.	H&V Units (O.A. Makeup)	5085	
3.	Preheat	6612	
4.	Reheat	7889	See Note #2
5.	Misc.		See Note #2

#### NOTES:

- Actual heating load associated with convectors is only 1080#/Hr. The remaining 4660 #/HR. is for freeze protection which would not be a serious concern at the reduced outside quantities anticipated in our final design.
- 2. Reheat load not additive simultaneously with other loads thus explaining why total does not match PRV sizing.



TABLE 2: EXISTING PUMPS

PUMP	SERVICE	<u>GPM</u>	<u>HP</u>	REMARKS
P-1	Chilled Water	1200	60	
P-2	11 11	1200	60	Standby
P-3	11 11	2400	100	•
P-4	Condenser Water	3000	125	
P-5	11 11	1500	60	
P-6	11 11	1500	60	Standby
P-7	Hotwell Cond.	50	3	
P-8	11 11	50	3	
P-9	11 11	30	3	
P-10	**	30	3	
P-11	Heating/C-1	46	2	
P-12	11	46	2	Standby
P-13	Heating/C-2	15	1/3	
P-14	'' /C-3	43	3/4	
P-15	Freeze Prot/C-4	63	1/4	
P-16	'' /C-5	830	15	



TABLE 3: AIR CONDITIONING UNITS

Unit #	Scheduled CFM	% of total	Location	Area Served	Remarks
1	34365	7.7	Penthouse	General	
2	42820	9.7	11	Area	
3	45500	10.4	11	111 6 8	
4	37760	8.6	11		
5	45730	10.4	11		
6	45600	10.4	11		
7	40810	9.3	11		
8	34060	7.8	11		
9	30860	7.0	11		
10	33600	7.7	11		
11	23600	5.3	Penthouse		
12*	17260	3.9	App. Rm. #4		
13*	4310	1.0	App. Rm. #4	Meeting Rms. 232, 233, 234 (off Balcony)	Multizone Package Unit
14*	2440	0.5	Coat Rm. #176	Administra- tion Area	Packaged Unit

### <u>Total Air</u>: 438715

## NOTES: (1) Scheduled CFM not

- (1) Scheduled CFM not intended to indicate existing.
- (2) Refer to Balancing Report for present operating CFM.
- (3) \* Units requiring removal due to new construction. In addition, at least one of the other 11 units will require removal. The anticipated remaining air capacity is 380,000 CFM±.



TABLE 4: MAINTENANCE COSTS

			% Increase Over Base Year	% Increase Over Previous Year
Base Year:	1977 :	\$ 82,461.46		
	1978	\$ 87,409.15	6 %	6 %
	1979	\$ 87,409.15		
	1980	\$ 87,409.15	~ ~ -	
	1981	\$139,000.00	68.5%	59%
	1982	\$154,140.00	86.9%	10.9%
	1983	\$199,500.00	141.9%	29.4%

TABLE 5: UTILITY OPERATING COSTS

STEAM			ELECTRIC				
IME PERIOD	COSTS	1000# USE	COST/ 1000#		COSTS	1000KW USE	COST/KW
ly 78 - June 79 ly 79 - June 80 ly 80 - June 81 ly 81 - June 82	\$173,178 \$201,307 \$164,651 \$134,139	23233 17566 12849 10061	\$ 7.45 \$11.46 \$12.81 \$13.33		\$237,027 \$311,880 \$333,589 \$413,581	4046 4096 3679 4343	5.8c 13.1c 11.8c 10.5c

OTES: Table 5 information is from 2 different sources (Boston Edison and Public Facilities Department) not exactly the same but were generally similar. Table is shown to indicate general trends.



# TABLE 6: PRELIMINARY AIR HANDLING UNIT CAPACITY REQUIREMENTS

Space Use	Areas	Air Conditioning Block Loading
Meeting Rooms Prefunction Exhibition	71,900 168,400 246,000	143,800 cfm 421,000 cfm 738,000 cfm
Support Totals	215,200 701,500 sq. ft. -10%	215,200 cfm 1,518,000 cfm - 151,800 System Diversity 1,366,200 cfm

Approximate Existing A.C. Air Handling Capacity to Remain (pending further study).

NEW AIR HANDLING CAPACITY

- 380,000 cfm (See Table #3 Note #3) 986,200 cfm

- VI. SUPPORT DOCUMENTATION, (Cont'd)
- B. PRELIMINARY AIR CONDITIONING CONSIDERATIONS
  - 1. ASHRAE NOTES ON CONVENTION CENTERS 1978 Applications Chapter #4 Page 4.6 1982 Applications Chapter #4 Page 4.7
    - a. Flexibility in system is key consideration due to variable use factor.
    - b. Industrial shows require highest load

This load is high because most equipment does not operate simultaneously.

c. Exhibition Space Recommended Capacities:

System should accommodate:

```
EQUIPMENT: (Misc.) 10 w/sq. ft.

LIGHTS: (from Lottero & Mason) 5 w/sq. ft.

PEOPLE: 40 sq. ft./person 2.2 w/sq. ft.

Totals. 17.2 w/sq. ft. = 58.7 btu/sq. ft. = 2.47 cfm/sq. ft.
```

- d. Determination of accurate occupancy and usage information is critical.
- e. Multi-speed fans or variable volume must be a strong consideration due to varying loads.
- f . Cooling coil selection should be made with the knowledge of highly variable latent load requirements.
- g. Special Requirements:
  - (1) Systems should be capable of operating on 100% QA because during set-up time trucks can sometimes be driven directly into the space.
  - (2) Space can be used to exhibit and operate equipment with funes, therefore, flues must be provided for direct removal of noxious odors.
- h. Storage rooms can often be indirectly air conditioned by exhausting (returning) excess air from the main hall through the storage space.



### VI. B. 2. Ventilation:

This facility will handle 8000 to 12000 people simultaneously.

ASHRAE standards for natural and mechanical ventilation are as follows:

Sq.		Sq. Ft./Person	CFM				
SPA	ACE DESCRIPTION	OCCUPANCY	MINIMUM	RECOM-ENDED			
1.	Auditoriums (no smoking)	7 sq. ft.	5	5 - 10			
2.	Lobbies (Foyers and Lounges)	7 sq. ft.	20	25 - 30			
3.	Kitchens	50 sq. ft.	30	35			
4.	Rest Roams	100 sq. ft.	15	20 - 25			
5.	Ballrooms	10 sq. ft.	15	20 - 25			
6.	Conference Rooms	17 sq. ft.	25	30 - 40			

# NOTES: 1. Values listed in table can be reduced to 33% by meeting Section 3 of ASHRAE Standard 62, but is no case less than 5 cfm/person.

Overall ventilation rate for the Hynes will be approximately 10 - 15% of the total air quantity listed in Table 6. 10% = 11.4 cfm/person for 12000 people.



# VI. B. 3. Review Of Hynes Space and Function Program - HVAC:

### 1. Exhibit Hall:

"Use ASHRAE standards for loads. Consider use of electrostatic filters for smoke and particle removal, which can dramatically reduce fresh air requirements and corresponding air conditioning tonnage. Consider statification of air delivery in high spaces, to deliver conditioned air only at occupied levels. Establish velocities of air delivery which will not unduly disturb hanging banners or displays. Smoke removal system may be required by code and is desirable. Provide heaters over external service doors."

### 2. Lobbies:

"Normal. Use 15 sq. ft./person for loads."

### 3. Banquet/Ballrooms:

'Use about 1 person per 11 sq. ft. for population loads. Consider use of electrostatic filters for smoke and particle removal, which can be dramatically reduce fresh air requirements and corresponding air conditioning tonnage. Consider stratification of air delivery, to condition only at occupied levels."

### 4. Meeting Rooms:

"Use about 1 person per 11 square feet for population loads. Consider use of electrostatic filters for smoke and particle removal, which can dramatically reduce fresh air requirements and corresponding air conditioning tonnage. High delivery and low return recommended Exhaust interconnected to delivery system recommended."

## 5. Prefunction:

"Use about 1 person per 15 square feet for population load."

# 6. Building Control Room:

"Building Automation Computer."





# THOMAS-YOUNG ASSOCIATES, INC.

ENERGY CONSERVATION ENGINEERS
617 MILL STREET — MARION, MASS. 02738
800-352-7166 617-748-0204

HYNES AUDITORIUM

BOSTON, MASSACHUSETTS

TESTING AND BALANCING REPORT

JUNE 1982

THOMAS-YOUNG ASSOCIATES

ADDRESS: BOSTON, MASSACHUSETTS DATE: JUNE 1982

#### SUMMARY OF AIR HANDLING UNITS

1 11 0000000000000000000000000000000000									
		SPECIFIED	)	ACTUAL					
UNIT NO.	1	RETURN	OSA	TOTAL	RETURN	OSA			
	CFM	CFM	CFM	CFM	CFM	CFM			
S - 1	34365	27475	6890	22222	19228	2994			
S-2	42820	20570	22250	22607	31302	0			
S-3	45500	36400	9100	19027	31959	0			
S - 4	37760	21390	16370	23939	29520	0			
s-5	45730	36580	9150	25163	17162	8001			
s-6	45600	36460	9140	30262	32866	0			
s-7	40810	31490	9320	21010	22094	0			
S-8	34060	13150	20910	25544	26879	. 0			
S = 9	30860	0	30860	27183	14497	12686			
S-10	33600	5100	28500	26110	18914	7196			
S-11	23600	18880	4720	18472	14291	18472			
S-12	17260	4040	13200	12678	14967	0			
S-13	4310	940	3 3 7 0	3951	2248	1703			
						<b>:</b>			
TOTAL	436275	252495	183780	278168	275927	51052			





# THOMAS-YOUNG ASSOCIATES

JOB NAME	HYNES	AUDITORIUM	
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BOSTON, MASSACHUSETTS

ADDRESS DONE 1/, 1982	A D I	DPFCC	JUNE	17,	1982
-----------------------	-------	-------	------	-----	------

DATE \_\_\_\_\_

#### AIR MOVING EQUIPMENT TEST SHEET

		NOVING E	OTPHENT	1531 581	LL1		
UNIT NO.	S-1				R-1		
LOCATION	Penthou	se	P		Pentho	Penthouse	
MANUFACTURE	America	American Standard				American	
MODEL NO.	6680			Standard *			
SERIAL NO.	274				*		
SIZE	330			-			
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	34365	22222				19228	
RETURN AIR C.F.M.	27475	19228					
0.S.A. C.F.M.	6890	2994					
TOTAL STATIC PRESSURE		5.92				1.97	
SUCTION PRESSURE		82				-1.9"	
DISCHARGE PRESSURE		+5.1				.07	
MOTOR H.P.	7 5	75			25	2 5	
VOLTAGE	480	480			480	480	
PHASE	3	3			3	3	
MOTOR RPM	1775	1775			1770	1770	
FAN R.P.M.	NL	1400			NL	620	
AMPERAGE	85	42/42/42			27.5	16/15/15	

B.H.P.

<sup>\*</sup>Nameplate not accessible - covered with insulation



Date \_\_ JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-1 BRANCH	A SI	ZE <u>16"</u>	AREA 1	.396 ACT	JAL SP 3.4
	1					
TRAVERSE NO.	1	2	3	4	5	6
1	3500					
2	3000					
3	2900					
4	2900					
5	2800					
6	2600					
7						
8						
TOTAL	19800					
AVERAGE	3300					
AV	ERAGE VELO	CITY =	3300	TOTAL CE	'M = '	1597

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S-	1 BRANCH	B-1 S	IZE <u>16"</u>	AREA _	396 ACT	UAL SP
TRAVERSE NO.	1	2	3	4	5	6
1	2100					
2	1950					
3	1950					
4	1950					
5	2000					
6		·				
7						
8						
TOTAL	9950					
AVERAGE	1990					
AVE	RAGE VELO	TTY =	1990	TOTAL CE	M = 277	8

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H)  
= Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S	-1 BRANCH	B-2 SI	ZE <u>18"</u>	_ AREA 1.3	767 ACT	JAL SP
TRAVERSE NO.	1	2	3	4	5	6
1	2500					
2	2500					
3	2700					
4	2800					
5	2900					
6						
7						
8						
TOTAL	13400					
AVERAGE	2680					
AV	ERAGE VELO	CITY =	2680	TOTAL C	FM = 4	736

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S	S-1 BRANCH	B-3 SI	ZE 22"	AREA 2	.64 ACT	JAL SP
	<del> </del>			,		
TRAVERSE NO.	1	2	3	4	5	6
1	1300					
2	1200					
3	1300					
4	1750		_			
5	1800					
6						
7						
8						
TOTAL	7350					
AVERAGE	1470					
AV	ERAGE VELO	CITY =	1470	TOTAL C	FM = 388	1

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)}{(2)} = Sq.Ft.$$



#### DUCT TRAVERSE READINGS

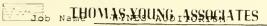
SYSTEM	S-1 BRANCH	B-4 S	IZE <u>22"</u>	AREA	2.64 ACT	JAL SP 4.1
TRAVERSE NO.	1	2	3	4	5	6
1	2600					
2	2200					
3	2100					
4	2100					
5	2800					
6						
7						
8						
TOTAL	11800					
AVERAGE	2360					
AV	ERAGE VELO	CITY =	2360	TOTAL C	FM = 6230	

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$





Date \_\_\_ JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	R1 BRANCH	Main SI	ZE 86x30	_ AREA _1	7.92 ACT	UAL SP27			
TRAVERSE NO.	1	2	3	4	5	6			
1	1200	1200	1300	1300	1300	1350			
2	1100	1300	1400	1400	1500	1500			
3	1100	1200	1300	1400	1400	1450			
4	1000	1200	1200	1300	1400	1400			
5	800	1100	1200	1300	1300	1250			
6	500	700	1000	1050	1200	1200			
7	500	500	700	800	800	900			
8	400	500	600	600	700	700			
TOTAL	6600	7700	8700	9150	9600	9750			
AVERAGE	825	963	1088	1144	1200	1219			
AV	AVERAGE VELOCITY = 1073 TOTAL CFM = 19228								

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

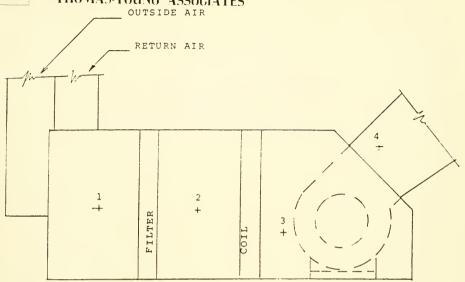
Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.





# THOMAS-YOUNG ASSOCIATES



#### UNIT TRAVERSE READINGS

#### SUPPLY FAN NO. 1

SP-1 -0.48

SP-2 -0.59

SP-3 0.82

SP-4 5.92





# THOMAS-YOUNG ASSOCIATES

#### JOB NAME HYNES AUDITORIUM

# ADDRESS BOSTON, MASSACHUSETTS DATE JUNE 16, 1982

#### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-2				R-2	
LOCATION			Penth	ouse		
MANUFACTURE		American Standard				ican dard
MODEL NO.	1-6680	0 <b>-</b> D			NA	
SERIAL NO.	365-73				NA.	`
SIZE	365			·	NA_	
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL
TOTAL C.F.M.	42820	-±22607				31,302
RETURN AIR C.F.M.	20570	31302				
O.S.A. C.F.M.	22250	0				
TOTAL STATIC PRESSURE		6.8				2.45
SUCTION PRESSURE		-0.40				-2.40
DISCHARGE PRESSURE		6.40:				+0.05
MOTOR H.P.	75	75			30	30
VOLTAGE	480	480			480	480
PHASE	3	3			3	3
MOTOR RPM	1775	1775			1770	1770
FAN R.P.M.	-NL	1340			NL	640
AMPERAGE	85	51/62/62			33	22/22/22

B.H.P.

Frame #

405U

326U

NOTE: Return is higher than supply air but supply is much less than design



# THOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	-2 BRANCH	<u>A-1</u> S	IZE <u>22"</u>	AREA 2.	64 ACT	JAL SP 4.90
TRAVERSE NO.	1	2	3	4	5	6
1	1600					
-2	1500					
3	1450					
4	1350					
5	1400					
6	1450					
7	1					
8						
TOTAL	8750					
AVERAGE	1458					
AVI	ERAGE VELO	CITY =	1458	TOTAL C	FM = 384	9

Rectangular Duct =  $w" \times H" = Sq.Ft$ .

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H")^2 + H" \times (W-H)}{(2)} = Sq.Ft.$$



#### DUCT TRAVERSE READINGS

SYSTEM S-	-2 BRANCH	_A-2 SI	ZE <u>16"</u>	AREA 1.	396 ACT	UAL SP 5.95
TRAVERSE NO.	1	2	3	4	5	6
1	1500					`
2	1300					
3	1300					
4	1300					
5	1300					
6	1500					
7						
8						
TOTAL	8200					
AVERAGE	1367					
AVI	ERAGE VELO	CITY =	1367	TOTAL CH	FM = 190	8

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



# THO WAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-2 BRANCH	B-1 SI	ZE <u>16"</u>	AREA 1.	396 ACT	UAL SP <u>6.20</u>
TRAVERSE NO.	1	2	3	4	5	6
1	1500					`
2	1450					
3	1400					
4	1400					
5	1400					
6	1400					
7						
8						
TOTAL	8550					
AVERAGE	1425					
AV	ERAGE VELO	CITY =	1425	TOTAL CI	M = 1989	)

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $R^2$ " = Sq.Ft.



THO MASSACHUSETTS BOSTON, MASSACHUSETTS

Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	-2 BRANCH	<u>B-2</u> S1	ZE _22"	AREA 2.	64 · ACTI	UAL SP <u>5.85</u>
TRAVERSE NO.	1	2	3	4	5	6
1	1600					
-2	1550					
3	1500					
4	1400					
5	1350					
6	1350					
7						
8						
TOTAL	8750					
AVERAGE	-1-458-					
AVI	ERAGE VELO	CITY =	1458-	TOTAL C	FM = 30.	19

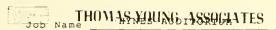
Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)} + H'' \times (W-H)}{(2)} = Sq.Ft.$ 





Date \_\_\_ JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	S-2 BRANCH	C-1 SI	ZE <u>18"</u>	AREA 1	1.767 ACT	JAL SP 1.75'
TRAVERSE NO.	1	2	3	4	5	6
1	2450					
2	2450					
3	2350					
4	2350					
5	2350					
6	1900					
7						
8						
TOTAL	13850					
AVERAGE	2308					
7A	ERAGE VELO	CITY =	2308	TOTAL C	FM =	78

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



# Job Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date \_\_JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	S-2 BRANCH	C-2 SI	ZE <u>18"</u>	AREA 1.	767 ACT	JAL SP 5.60
TRAVERSE NO.	1	2	3	4	5	6
1	2300					
2	2200					
3	2200					
4	2300					
5	2300					
6	1400					
7						
8						
TOTAL	12700					
AVERAGE	2116					
AV	ERAGE VELO	CITY =	2116	TOTAL C	FM =37	39

Formula for calculation area:

Rectangular Duct =  $W'' \times H'' = Sq.Ft$ .

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



5 ''

Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-2 BRANCH	<u>C-3</u>	SIZE	18'	_ AREA _1	.767 ACT	UAL SP
TRAVERSE NO.	1	2		3	4	5	6
1	2050						
2	1950						
3	1900						
4	1800						
5	1600						
6	1550						
7		-					
8							
TOTAL	10850				_		
AVERAGE	1808						
AV	ERAGE VELO	CITY =		1808	TOTAL C	FM = 3195	

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H")^2 + H" \times (W-H)}{(2)}$$
 = Sq.Ft.



Date JUNE 22, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R-	2 BRANCH	Main SI	ZE <u>80x40</u>	AREA 22	.2 ACT	UAL SP <u>0.16</u>
TRAVERSE NO.	1	2	3	4	5	6
1						
1	800	1100	1400	1750	1900	1900
· 2	900	1000	1400	1700	1800	1950
3	900	1000	1450	1600	1800	1900
4	850	1100	1400	1600	1750	1900
5	900	1000	1400	1500	1750	1800
6						
7						
8						
TOTAL	4350	5200	7050	8150	8100	9450
AVERAGE	870	1040	1410	1630	1620	1890
AVI	ERAGE VELO	CITY =	1410	TOTAL C	FM = 313	0.2

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

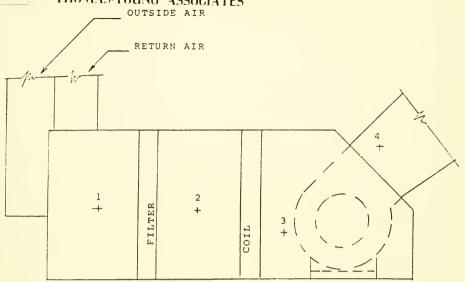
Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.





## THOMAS-YOUNG ASSOCIATES



#### UNIT TRAVERSE READINGS

#### SUPPLY FAN NO. 2

SP-1 -0.23

SP-2 -0.26

SP-3 0.40

SP-4 6.40



## THOMAS-YOUNG ASSOCIATES

JOB NAME	HYNES AUDITORIUM	BOSTON, MASSACHUSETTS
ADDRESS		DATE _JUNE 16, 1982

### AIR MOVING EQUIPMENT TEST SHEET

	.,						
UNIT NO.	S-3				R-3		
LOCATION			Penth	ouse			
MANUFACTURE	n	American Standard			Ameri Stand		
MODEL NO.	1-66800	) – D		1-66800-1			
SERIAL NO.	365-73				542-10		
SIZE	365				542		
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	45500	19027 -				31959	
RETURN AIR C.F.M.	36400	31959					
O.S.A. C.F.M.	9100	0					
TOTAL STATIC PRESSURE		8.39				2.65	
SUCTION PRESSURE		-0.49				-3.1	
DISCHARGE PRESSURE		+7.9"				-0.45	
MOTOR H.P.	75	75			30	30	
VOLTAGE	480	480			480	480	
PHASE	_3	3			3	3	
MOTOR RPM	1775	1775			1770	1770	
FAN R.P.M.	NI	1380			NL.	- 700	
AMPERAGE	85 6	0/60/60			3 3	35/36/36	

FRAME # 405U

326U

NOTE: Return is higher than supply. Supply is much less than design



## THOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM _	S-3 BRANCH	<u>A-1</u> SI	ZE <u>22"</u>	AREA _2	640 ACT	UAL SP 2.6
TRAVERSE NO.	1	2	3	4	5	6
1	2150					`
2	1850					
3	1450					
4	1800					
5	1650					
6	1400					
7						
8						
TOTAL	10300					
AVERAGE	1717					
/ - 317	EDACE METO	TMV -		TOTAL CI	2 M -	

AVERAGE VELOCITY = 1717 TOTAL CFM = 4533

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	BRANCH	<u>A-2</u> SI	ZE <u>22</u>	AREA _2	.64 ACT	UAL SP 2.7
TRAVERSE NO.	1	2	3	4	5	6
1	1400					`
-2	1500					
3	1650					
4	1750					
5	1700					
6	1900					
7						
8						
TOTAL	9900					
AVERAGE	1650					
AVI	ERAGE VELO	CITY =	1650	TOTAL CF	M = .4356	

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



# THOMAS-YOUNG ASSOCIATES HYNES AUDITORIUM

Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

BOSTON, MASSACHUSETTS

SYSTEM S	-3 BRANCH	_A-3_ SI	ZE 22"	AREA 2.	640 ACT	JAL SP 3.6
	1	1	1			
TRAVERSE NO.	1	2	3	4	5	6
	-					
1	1400					
2	1400					
3	1600					
4	1650					
5	1700					
6	2000					
7						
8						
TOTAL	8720					
AVERAGE	1458					
AV	ERAGE VELO	CITY =	1458	TOTAL CI	M = 3849	

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$

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THOMAS-YOUNG ASSOCIATES

JOB Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	-3 BRANCH	<u>A-4</u> SI	ZE 22*	AREA 2.	640 ACT	JAL SP +2.8
TRAVERSE NO.	1	2	3	4	5	6
1	2200					
2	1950					
3	1700					
4	1600					
5	1650					
6	1700					
7						
8						
TOTAL	10800					
AVERAGE	1800					
AV	ERAGE VELO	CITY =	1800	_ TOTAL C	FM = 47	5 2

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



Date \_\_\_JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-3 BRANCH	B SI	ZE <u>14"</u>	AREA 1.	069 ACT	JAL SP +1.2
TRAVERSE .	1	2	3	4	5	6
1	1400					
2	1400					
3	1400					
4	1400					
5	1400					
6	1400					
7						
8						
TOTAL	8400					
AVERAGE	1400					
AV	ERAGE VELO	CITY = J	1400	TOTAL C	FM = 1537	7

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 22, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R-	-3 BRANCE	Main Si	ZE1 <u>34"x33</u>	" AREA 30	).7ft ACT	UAL SP	+0.07
TRAVERSE NO.	1	2	3	4	5	6	7
1	1100	1250	1200	1300	900	800	500
.2	1300	1350	1300	1500	1000	700	500
3	1300	1500	1400	1550	1000	600	400
4	1300	1450	1400	1600	900	600	400
5	1250	1400	1200	1550	700	500	400
6	900	1300	1450	1500	500	600	400
7							
8							
TOTAL	7150	8250	7950	9000	5000	3800	2600
AVERAGE	1192	1375	1325	1500	833	633	433
AVE	ERAGE VELC	CITY =	1041	TOTAL C	FM = 3105	. 0	

Formula for calculation area:

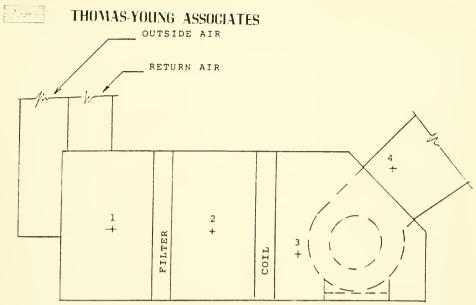
Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)} + H'' \times (W-H)$  = Sq.Ft.







### UNIT TRAVERSE READINGS

### SUPPLY FAN NO. 3

SP-1 -0.22

SP-2 0.29

SP-3 0.49

SP-4 +7.9





## THOMAS-YOUNG ASSOCIATES

JOB NAME HYNES AUDITORIUM

ADDRESS BOSTON, MASSACHUSETTS DATE JUNE 16, 1982

### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-4				R-4		
LOCATION			Pentho	use			
MANUFACTURE	Americ					American Standard	
MODEL NO.	668000	:				1-66800C	
SERIAL NO.	274					490-10	
SIZE	330				490		
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	37760	23939				29520	
RETURN AIR C.F.M.	21390	29520					
O.S.A. C.F.M.	16370	0					
TOTAL STATIC PRESSURE		6.50				1.82	
SUCTION PRESSURE		-0.60				-2.10	
DISCHARGE PRESSURE		+5.90				28	
MOTOR H.P.	75	75			25	25	
VOLTAGE	480	480			280	280	
PHASE	3	3			3	3	
MOTOR RPM	1775	1,775			1770	1770	
FAN R.P.M.	NL	1460			NL	620	
AMPERAGE	85	45/45/45			27.5	19/18/18	

B.H.P.



Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	4 BRANCH	<u>A-1</u> SI	ZE <u>18"</u>	AREA 1.7	67 ACT	JAL SP 1.9"	
		,	ŀ	1			
TRAVERSE ·	1	2	3	4	5	6	
1	1900						
2	1600						
3	1300						
4	1200						
5	1300						
6	1300						
7							
8							
TOTAL	8600						
AVERAGE	1433						
AUI	AVERAGE VELOCITY = 1433 TOTAL CFM = 2532						

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H)  
= Sq.Ft.





# THOMAS YOUTNGRASSOCIATES

Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	4 BRANCH	A2 SI	ZE	AREA 2.	640 ACT	JAL SP 3.6"
TRAVERSE NO.	1	2	3	4	5	6
1	2800					
2	2800					
3	2750					
4	2700					
5	2800					
6	2800					
7	2700					
8						
TOTAL	19350					
AVERAGE	27.6/4					
AV	ERAGE VELO	CITY = 2	693	TOTAL CI	FM = 729	7

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



# THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM

BOSTON, MASSACHUSETTS

Date \_\_\_\_ JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-4 BRANCH	<u>B-1</u> SI	ZE <u>22"</u>	AREA _2	.64 ACT	UAL SP _+2.8
TRAVERSE NO.	. 1	2	3	4	5	6
1	3600					
2	3500					
3	3200					
4	2600					
5	2550					
6						
7						
8						
TOTAL	15450					
AVERAGE	3090					
· AV	ERAGE VELC	CITY =	3090	TOTAL C	FM = 815	8

Formula for calculation area:

Rectangular Duct = W" x H" = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-4 BRANCH B-2 SIZE 22 AREA 2.64 ACTUAL SP 0.2"						
TRAVERSE NO.	1	2	3	4	5	6
1	1500					
2	1500			_		
3	1500					
4	1500					
5	1550					
6	1550					
7	1550					
8	1550					
TOTAL	12200					
AVERAGE	1525					
AVERAGE VELOCITY = 1525 TOTAL CFM = 4026						

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date \_\_\_ JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	4 BRANCH	B-3 SI	ZE <u>10"</u>	AREA	545 ACT	JAL SP 3 9	
		1	i -	1	1	i	
TRAVERSE .	1	2	3	4	5	6	
1	ļ						
	1300						
2	1900						
3	2100						
4	2200						
5	2300						
6							
7							
8							
TOTAL	9800						
AVERAGE	1960						
AVERAGE VELOCITY = 1960 TOTAL CFM = 1070							

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	4 BRANCH	C' SI	ZE <u>10"</u>	AREA .5	45 ACT	JAL SP 4.8"
TRAVERSE .	1	2	3	4	5	6
1	1550					
2	1700					
3	1700					
4	1650					
5	1650					
6						
7						
8						
TOTAL	7850					
	1570					
` AV	ERAGE VELO	CITY =	1570	TOTAL C	FM = 856	

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



## Job

## THOMAS-YOUNG ASSOCIATES Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date \_\_\_ JUNE 22, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R-	4 BRANCH	MAIN SI	ZE4 <u>8x72</u>	AREA24f	t <sup>2</sup> ACT	UAL SP	3:
TRAVERSE NO.	1	2	3	4	5	6	
1	1200	1300	200	1150			_
2	1300	1200	1250	1200			
3	1300	1200	1250	1120			
4	1250	1300	1200	1200			_
5	1300	1300	1200	1200			
6	1350	1200	1250	1150			_
7	1250	1200	1250	1100			
8							
TOTAL	8950	8700	8600	8200		<del></del>	
AVERAGE	1278	1243	1228	1171			
AVI	ERAGE VELO	CITY =	1230	TOTAL C	FM = 2952	0	_

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

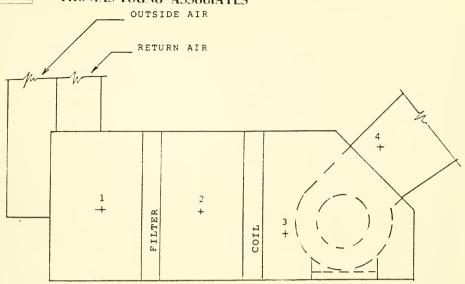
Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$

2 "







### UNIT TRAVERSE READINGS

#### SUPPLY FAN NO. 4

SP-1 -.19

SP-2 .31

SP-3 0.60

SP-4 5.9





JOB	NAME_	HYNES	AUDITORIUM	BOSTON,	MASSACHUSETTS
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ADDRESS DATE JUNE 15, 1982

#### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-5			R-5				
LOCATION			Penth	Penthouse				
MANUFACTURE	Americ				Americ			
MODEL NO.	1-6680	0-D				0-1		
SERIAL NO.	365-73				542-10			
SIZE 365 542								
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL		
TOTAL C.F.M.	45730	25163				17162		
RETURN AIR C.F.M.	36580	17162						
O.S.A. C.F.M.	9150	8001						
TOTAL STATIC PRESSURE		4.24				1.73		
SUCTION PRESSURE		-0.64				-1.65		
DISCHARGE PRESSURE		3.60				+.08		
MOTOR H.P.	75	75			30	30		
VOLTAGE	480	480			480	4.80		
PHASE	3	3			3	3		
MOTOR RPM	1775	1775			1770	1770		
FAN R.P.M.	NL	1220			NL ·	640		
AMPERAGE	85	48/48/48			33	19/19/19		

B.H.P.



Date JUNE 14, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-5 BRANCH	<u>A-1</u> SI	ZE <u>16"</u>	AREA 1.	396 ACT	UAL SP 3.7
TRAVERSE NO.	. 1	2	3	4	5	6
1	1650					
2	1700					
3	1800					
4	1800					
5	1800					
6	1750					
7	1					
8						
TOTAL	10500					
AVERAGE	1750					
ΑV	ERAGE VELO	CITY =	1750	TOTAL C	FM = 244	3

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.





## THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM

BOSTON, MASSACHUSETTS

Date JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-5 BRANCH A-2 SIZE 18 AREA 1.767 ACTUAL SP 3.25								
TRAVERSE NO.	1	2	3	4	5	6		
1	2050							
2	2050							
3	2100							
4	2100							
5	2000							
6	1950							
7					·			
8								
TOTAL	12250							
AVERAGE	2042							

AVERAGE VELOCITY = 2042 TOTAL CFM = 2 3608

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.





## THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM

BOSTON, MASSACHUSETTS

Date JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-5 BRANCH B-1 SIZE 18" AREA 1.767 ACTUAL SP 3.3							
TRAVERSE ·	1	2	3	4	5	6	
1	2600						
2	2600						
3	2600						
4	2500						
5	2400						
6	2400						
7							
8					-		
TOTAL	15100						
AVERAGE	2517						
AV	ERAGE VELO	CITY =	2517	TOTAL C	FM = 4448		

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H^*)^2 + H^* \times (W-H)}{(2)}$$
 = Sq.Ft.



# THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date \_ JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-5 BRANCH	<u>B-2</u> 5I	ZE	AREA j.	.767 ACT	JAL SP 3.35
TRAVERSE NO.	1	2	3	4	5	6
1	2300					
2	2100					
3	2100					
4	1950					
5	1750					
6	1680					
7						
8						
TOTAL	11850					
AVERAGE	1975					
AV	ERAGE VELO	CITY =	1975	TOTAL C	FM =34	90

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H)  
= Sq.Ft.



Date \_\_\_JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-5 BRANCH	B-3 SI	ZE 18"	AREA 1.	767 ACT	JAL SP 3.2
TRAVERSE :	1	2	3	4	5	6
1	2000					
`2	1900					
3	1900					
4	1750					
5	1700					
6	1700					
7						
8						
TOTAL	10950					
AVERAGE	1825					
AV	ERAGE VELO	CITY =	1825	TOTAL CI	M = .3225	5

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	5 BRANCH	B-4 SI	ZE	AREA 2.	182 ACT	JAL SP 3.1
TRAVERSE ·	1	2	3	4	5	6
1	2250					
`2	2100					
3	2150					
4	2100					
5	2200	<u>-</u>				
6	2300					
7						
8						
TOTAL	13100					
AVERAGE	2183					
AVI	ERAGE VELO	CITY =	2183	TOTAL C	FM = 476	3

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



Date JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-5 BRANCH B-5 SIZE 16" ARE? 1.396 ACTUAL SP 3.4								
TRAVERSE NO.	1	2	3	4	5	6		
1	1550							
`2	1250							
3	1200							
4	1300							
5	1400							
6	1300							
7								
8								
TOTAL	8000							
AVERAGE	1333							
AV	ERAGE VELO	CITY =	1333	TOTAL C	FM = 1861			

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



## THOMAS YOUNG ASSOCIATES Job Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date JUNE 15, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-5 BRANCH C SIZE 18" AREA 1.767 ACTUAL SP 1.3							
TRAVERSE NO.	1	2	3	4	5	6	
1	800						
2	900						
3	800						
4	700						
5	700						
6	600						
7							
8							
TOTAL	1500						
AVERAGE	750						
AV	ERAGE VELO	CITY =	750	TOTAL CI	FM - <u>132</u> 5		

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' × (W-H)  
= Sq.Ft.





# THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM BOSTON, MASSACHUSETTS

Date \_\_\_ JUNE 16, 1982

#### DUCT TRAVERSE READINGS

		1				
TRAVERSE NO.	1	2	3	4	5	6
1	600					
`2	400					
3	400					
4	400					
5	400					
6	400					
7	300					
8	300					
OTAL	3200					
VERAGE	400					

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date \_\_ JUNE 16, 1982

#### DUCT TRAVERSE READINGS

SYSTEM F	-5 BRANCH	B SI	ZE <u>50x24</u>	AREA 8	.33 ACT	JAL SP0.81
TRAVERSE .	1	2	3	4	5	6
1	800					
2	1100					
3	1100					
4	700					
5	500					
6	500					
7	750				·	
8	800					
TOTAL	6300					
AVERAGE	784					

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 16, 1982

#### DUCT TRAVERSE READINGS

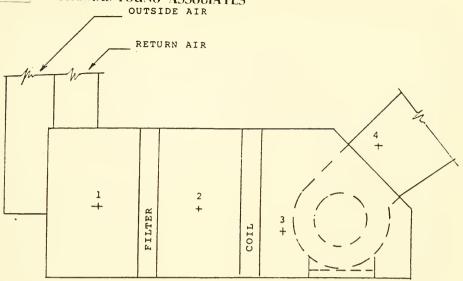
SYSTEM R-	5 BRANCH		ZE 25×49	AREA 8.5	507 ACT	JAL SP <u>-0.86</u>
TRAVERSE NO.	1	2	3	4	5	6
1	600					
2	600		-			
3	650					
4	600					
5	600					
6	700					
7	650					
8	600					
TOTAL	5000					
AVERAGE	625					

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$





#### UNIT TRAVERSE READINGS

49

SUPPLY FAN NO. 5

SP-1 0.27

SP-2 -0.30

SP-3 -0.54

SP-4 3.6



JOB NAME HYNES AUDITORIUM

ADDRESS BOSTON, MASSACHUSETTS DATE JUNE 15, 1982

### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-6				R-6			
LOCATION			Penth	Penthouse				
MANUFACTURE	America Standa:				- 1	American Standard		
MODEL NO.	1-66800	D-D				1-66800-1		
SERIAL NO.	365-73			600-57				
SIZE	365				600			
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL		
TOTAL C.F.M.	45600	32062			3286	6		
RETURN AIR C.F.M.	36460	32866						
O.S.A. C.F.M.	9140	0						
TOTAL STATIC PRESSURE		4.95				2.51		
SUCTION PRESSURE		-0.65				-2.30		
DISCHARGE PRESSURE		4.30			-	+0.21"		
MOTOR H.P.	75	75			25	_25		
VOLTAGE	48	480			480	480		
PHASE -	3	3 .			3	3		
_ MOTOR ,RPM	1775	1775_			1770	1770		
FAN R.P.M.	NL	1200			NL	540		
AMPERAGE	85 4	5/46/46			27.5	23/22/22		

B.H.P.

FRAME #

405U

324U



### DUCT TRAVERSE READINGS

SYSTEM S	-6 BRANCH	A-1 SI	ZE <u>18"</u>	AREA 1.	767 ACT	JAL SP 3.6"
TRAVERSE NO.	1	2	3	4	5	6
1	3100					
2	3100					
3	2900					
4	2900					
5	3200					
6	3150					
7						
8						
TOTAL	18350					
AVERAGE	3058					
AV	ERAGE VELO	CITY =	3058	TOTAL CI	M = 540	3

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



Date \_\_\_\_JUNE 16, 1982

### DUCT TRAVERSE READINGS

SYSTEM S	5-6 BRANCH	A-2 si	ZE 22"	AREA	2.64 ACT	JAL SP 3.9
TRAVERSE .	1	2	3	4	5	6
1	2400					
.2	2350					
3	2300					
4	2200					
5	2150					
6	2250					
7	2400					
8	2600					
TOTAL	18650					
AVERAGE	2331.					<del></del>
. AV	ERAGE VELO	CITY = 2	331	TOTAL C	FM = 61	54

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



### DUCT TRAVERSE READINGS

SYSTEM _S	-6 BRANCH	A-3 SI	ZE 16"	AREA .	1.40 ACT	JAL SP 3.6"
TRAVERSE NO.	. 1	2	3	4	5	6
1 .	2750					
2	2800					
3	2850					
4	2800					
5	2800					
6	2800					
7	2800					
8	2800					
TOTAL	22400					
AVERAGE	2800					
JA.	ERAGE VELO	CITY =	2800	TOTAL C	FM = 3	920

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



### DUCT TRAVERSE READINGS

SYSTEM S	-6 BRANCH	A-4 SI	ZE	AREA 1.	40 ACT	UAL SP 3.9
TRAVERSE NO.	1	2	3	4	5	6
1	2300					
2	2250					
3	2200					
4	2100					
5	2100					
6	2100					
7						
8						
TOTAL	13050					
AVERAGE	2175					
AV	ERAGE VELO	CITY = 2	175	TOTAL C	FM = 30	45.

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



### DUCT TRAVERSE READINGS

SYSTEM S-	6 BRANCH	A-5 SI	ZE	AREA 2.	64 ACT	JAL SP 3.3"
TRAVERSE .	1	2	3	4	5	6
1	2600					
2	2300					
3	2000					
4	1900					
5	2000					
6	2400					
7	2700					
8	2700					
TOTAL	18600					
AVERAGE	2325, .					

AVERAGE VELOCITY = 2325 TOTAL CFM = 6138

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



Date \_\_ JUNE 16, 1982

### DUCT TRAVERSE READINGS

SYSTEM S-	6 BRANCH	<u>A-6</u> SI	ZE <u>16"</u>	AREA 1	396 ACT	JAL SP 4.3"
TRAVERSE NO.	1	2	3	4	5	6
1 .	1500					
.2	1700					
3	1650					
4	1600					
5	1550					
6	1550					
7						
8						
TOTAL	9550					
AVERAGE	1592					
AV	ERAGE VELO	CITY =	1592	TOTAL C	FM = 2	222

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' × (W-H)  
= Sq.Ft.



### DUCT TRAVERSE READINGS

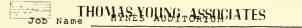
SYSTEM	S-6 BRANCH	A-7 SI	ZE <u>18"</u>	AREA 1.	767 ACT	JAL SP
TRAVERSE NO.	1	2	3	4	5	6
1	1650					
2	1800					
3	1900					
4	1950					
5	2000					
6	2100					
7	2100					
8	1800					
TOTAL	5300					
AVERAGE	1913					
AV	ERAGE VELO	CITY =	1913	TOTAL C	FM = 3380	0_

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = 5q.Ft.





Date JUNE 22, 1982

### DUCT TRAVERSE READINGS

SYSTEM R-	6 BRANCE	Main SI	ZE134x30	_ AREA	27.9 ACT	UAL SP 0.14
TRAVERSE NO.	1	2	3	4	5	6
		-				
1	1750	1850	1900	2000	1500	1300
-2	1750	1700	1500	1800	1100	1200
3	1700	1100	800	1100	500	1000
4	1500	600	500	600	500	800
5	1000	1500	700	500	800	800
6						
7						
8					·	
TOTAL	7700	6750	5400	6000	4400	5100
AVERAGE	1540	1350	1080	1200	880	1020
AV	ERAGE VELO	CITY =	1178	TOTAL C	FM = 328	366

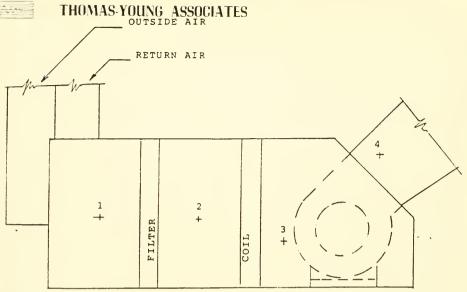
Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.







UNIT TRAVERSE READINGS

### SUPPLY FAN NO. 6

SP-1 -0.38

SP-2 0.35

SP-3 -0.65

SP-4 +4.30





## THOMAS-YOUNG ASSOCIATES

JOB NAME	HYNES AUDITORIUM	BOSTON,	MASSACHUSETTS
ADDDECC		TIME	16 1000

### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-7				R-7	
LOCATION		F		use		
MANUFACTURES	Americ			-		can
MODEL NO.	1-6680	0 <b>-</b> D			1-6680	
SERIAL NO.	365-73				402-19	)
SIZE	365				402	
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL
TOTAL C.F.M.	40810	21010				22094
RETURN AIR C.F.M.	31490	22094				
O.S.A. C.F.M.	9320	0				
TOTAL STATIC PRESSURE		6.18				2.73
SUCTION PRESSURE		-0.38				-1.80"
DISCHARGE PRESSURE		5.80				+0.93
MOTOR H.P.	75	75			25	25
VOLTAGE	480	480			480	480
PHASE	3	3			3	
MOTOR RPM	1775	1775			1770	1770
FAN R.P.M.	NL	1250			NL .	830
AMPERAGE	85	46/47/46			27.5	24/19/24

В.Н.Р.



Date \_\_\_\_\_JUNE 16, 1982

### DUCT TRAVERSE READINGS

SYSTEM S	-7 BRANCH	_A SI	ZE <u>18"</u>	AREA 1.	767 ACT	JAL SP 1.2"	
TRAVERSE NO.	1	2	3	4	5	6	
1	1900						
2	1900						
3	1850						
4	1850						
5	1900						
6	1950						
7							
8					1		
TOTAL	11350						
AVERAGE	1891						
AV	AVERAGE VELOCITY = 1891 TOTAL CFM = 3341						

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



# Job Nam THOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date \_\_\_\_\_JUNE 16, 1982

### DUCT TRAVERSE READINGS

SYSTEM S	-7 BRANCH	<u>B-1</u> SI	ZE 22"	AREA 2.	64ft ACT	JAL SP 5.5
TRAVERSE NO.	1	2	3	4	5	6
1	1700					
-2	1700					
3	1750					
4	1750					
5	1750					
6	1800					
7						
8	·				·	
TOTAL	10450		=			
AVERAGE	1742					
AV	ERAGE VELO	CITY =	1742	TOTAL CI	M = 459	9

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



### DUCT TRAVERSE READINGS

SYSTEM S	-7 BRANCH	B-2 SI	ZE	AREA2.6	4ft ACT	JAL SP 5.8
TRAVERSE NO.	1	2	3	4	5	6
1	1750					
-2	1700					
3	1700					
4	1700					<del></del>
5	1700					
6	1650					
7						
8	·					
TOTAL	10200					
AVERAGE	1700		1700		PM = 4488	

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$R^2$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H)  
= Sq.Ft.



### DUCT TRAVERSE READINGS

SYSTEM	S-7BRANCH	B-3 S	IZE	AREA .	2.182 ACT	UAL SP 5.8
TRAVERSE NO.	1	2	3	4	5	6
1	1000					
-2	1050					
3	1100					
4	1100					· · · · · · · · · · · · · · · · · · ·
5	1100					
6						
7						
8	·					
TOTAL	5350				-	
AVERAGE	1070					
AV	ERAGE VELO	CITY =	1070	TOTAL C	FM = 2335	

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



### DUCT TRAVERSE READINGS

2 2	1		1	1	-	
2 2		2	3	4	5	6
3	3000					
3 2	2900					
	2800					
4 2	2850					
5 2	2850					
6						
7						
8			=			
TOTAL 14	4400				-	==
AVERAGE 2	2880					

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



### DUCT TRAVERSE READINGS

-7 BRANCH	sı	ZE 12"	AREA .78	Bft <sup>2</sup> ACT	JAL SP 4.8
1	2	3	4	5	6
2800					
2800					•
2800					
2900					
2900					
14200	8				
2840					
	2800 2800 2800 2900 2900 14200 2840	1 2  2800 2800 2800 2900 2900 14200 2840	1 2 3  2800 2800 2800 2900 2900 14200 2840	1 2 3 4  2800 2800 2800 2900 2900 14200 2840	2800 2800 2800 2900 2900 14200 2840

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



Date \_\_\_ JUNE 22, 1982

### DUCT TRAVERSE READINGS

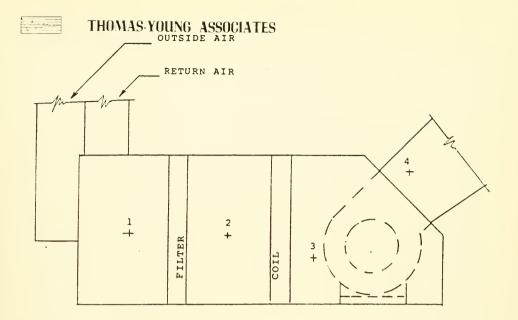
SYSTEM R-	-7 BRANCH	Main SI	ZE <u>78x36</u>	_ AREA <u>19</u>	.5ft <sup>2</sup> ACT	UAL SP -0 36
TRAVERSE NO.	1	2	3	4	5	6
1	900	900	1100	1100	1700	
-2	900	900	1150	1200	1600	
3	800	900	1150	1250	1600	
4	800	900	1200	1200	1500	
5	1000	1000	1100	1100	1400	
6	1000	900	1300	1000	1450	
7					•	
8	·				-	
TOTAL	5400	5500	8000	6850	8250	
AVERAGE	900	917	1333	1142	1375	
AV	ERAGE VELC	CITY =	11133	TOTAL C	FM =	974

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.





UNIT TRAVERSE READINGS

SUPPLY FAN NO. 7

The state of the s

SP-1 -0.06

SP-2 -0.11

SP-3 -0.38

SP-4 5.8





## THOMAS-YOUNG ASSOCIATES

JOB NAME\_\_\_ HYNES AUDITORIUM

ADDRESS BOSTON, MASSACHUSETTS DATE JUNE 23, 1982

### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-8			R-8			
LOCATION	Pentho	ıse			Pentho	enthouse	
MANUFACTURE	America				Americ		
MODEL NO.	66800-1	3			*		
SERIAL NO.	445-89				*		
SIZE 445 *							
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	34060	25544				26879	
RETURN AIR C.F.M.	13150	26879					
0.S.A. C.F.M.	20910	0 .					
TOTAL STATIC PRESSURE		6.24					
SUCTION PRESSURE		-0.69		_			
DISCHARGE PRESSURE		5.55					
MOTOR H.P.	60	60			25	25	
VOLTAGE	480	480			480	480	
PHASE	3	3			3	3	
MOTOR RPM	1775	1775	•		1770	1770	
FAN R.P.M.	NL	1060			NL ·	740	
AMPERAGE	70	14/44/44			27.5	6/15/15	

B.H.P.

\*Not Accessible



Name THO MAS YOUNG CASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	8 BRANCH	A SI	ZE <u>14"</u>	AREA 1	.07 ACT	JAL SP 5.2"
	-	1	1	1	1	1
TRAVERSE NO.	1	2	3	4	5	6
1	1850					
2	1900					
3	1800					
4	1750					
5	1700					
6	1700					
7						
8	·				-	
TOTAL	10700		8			
AVERAGE	1783					
AV	ERAGE VELC	CITY =	1783	TOTAL C	FM = 19	08

Formula for calculation area:

Rectangular Duct =  $\frac{W^* \times H^*}{144}$  = Sq.Pt.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$ 



#### DUCT TRAVERSE READINGS

SYSTEM S-	8 BRANCH	Bl SI	ZE <u>12</u>	AREA	785 ACT	JAL SP 4.5
		<u> </u>		1	<u> </u>	1
TRAVERSE NO.	1	2	3	4	5	6
1						
1	1300					
-2	1300					
3	1300					
4	1300					
5	1350					
6	1400					
7						
8						
TOTAL	7950					
AVERAGE	1325					
A 17	EDACE VELO	CITY =	1325	TOTAL C	EM = 10	10

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H")^2}{(2)} + H" \times (W-H)$$
 = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM	S-8 BRANCH	B2 SI	ZE <u>14"</u>	_ AREA _	1.07 ACT	JAL SP 4.0
TRAVERSE NO.	1	2	3	4	5	6
1	2800					
-2	2700					
3	2650					
4	2650					
5	2700					
6	2700					
7						
8						
TOTAL	116200					
AVERAGE	2700			-		
AV	ERAGE VELO	CITY =	2700	TOTAL C	CFM = 28	89

Formula for calculation area:

Rectangular Duct =  $\frac{W \times H^{*}}{144}$  = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



Date \_\_\_ JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	S-8 BRANCH	Cl si	ZE	_ AREA _	2.18 ACT	JAL SP 4.3"
TRAVERSE NO.	1	2	3	4	5	6
1	2600					
·2	2650					
3	2650					
4	2650					
5	2650					
6	2650					
7						
8						
TOTAL	15850					
AVERAGE	2642					
7.37	ERAGE VELO	CITY =	2642	TOTAL (	CFM = 57	6.0

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



Date \_\_\_ JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	S-8BRANCH	<u>C2</u> SI	ZE <u>20"</u>	AREA 2	.18 ACT	UAL SP 4.10
TRAVERSE NO.	1	2	3	4	5	6
1	3100					
2	3150					
3	3150					
4	3050					
5	2950					
6	2800					
7						
8						
TOTAL	18200					
AVERAGE	3033					
AV	ERAGE VELO	CITY =	3033	TOTAL C	FM = 6	612

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



Date \_\_\_JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-8 BRANCH	si	ZE <u>12</u>	AREA _7	R54 ACT	JAL SP 3.9"
TRAVERSE NO.	1	2	3	4	5	6
1	2700					
-2	2750					
3	2850					
4	2900					·
5	2850					
6	2850					
7						
8						
TOTAL	16900					
AVERAGE	2817					
AV	ERAGE VELO	CITY =	2817	TOTAL CH	M = 22	1 2

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



Date \_\_\_\_\_JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-8 BRANCH	E SI	ZE 20"	AREA 2	18 ACT	JAL SP 2.5	
TRAVERSE NO.	1	2	3	4	5	6	
1	2900						
2	2500						
3	2350					·	
4	2150						
5	2100						
6	2100						
7							
8							
TOTAL	14100						
AVERAGE	2350						
AV	AVERAGE VELOCITY = 2350 TOTAL CFM = 5123						

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)} + H'' \times (W-H)$  = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM R	-8 BRANCH	<u>1</u> si	ZE 23x34½'	AREA	5.51 ACT	JAL SP0.61
TRAVERSE NO.	1	2	3	4	5	6
1	1300					
-2	1300					
3	1300					
4	1300					
5	1250					
6	1300					
7	1200					
8	1100					
TOTAL	10050					
AVERAGE	1256					
AV	ERAGE VELO	CITY =	1256	TOTAL CI	FM = 69	120

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



Date \_\_\_ JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R-	8 BRANCH	s :	ZE <u>24x50</u>	AREA	8.33 ACT	JAL SPO_65
TRAVERSE NO.	1	2	3	4	5	6
1	1200					
-2	1200					
3	1100					
4	1400					
5	1500					
6	1200					
7	1000					
8						
TOTAL	8600					
AVERAGE	1229					
AVERAGE VELOCITY = 1229 TOTAL CFM = 10,237						

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



## Job Name THO MAS YOUNG ASSOCIATES

BOSTON, MASSACHUSETTS

Date \_\_\_JUNE 17, 1982

#### DUCT TRAVERSE READINGS

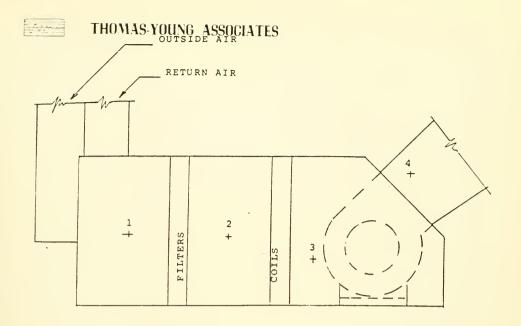
SYSTEM R-	8 BRANCH	3 SI	ZE 22x46	_ AREA7	.03 ACT	JAL SP0_95
TRAVERSE NO.	1	2	3	4	5	6
1	600					
2	1500					
3	1750					
4	1600					
5	1400					
6	1450					
7						
8						
TOTAL	8300					
AVERAGE	1383					
AVE	RAGE VELO	CITY =	1383	TOTAL CI	M = 9722	

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.





# UNIT TRAVERSE READINGS

## SUPPLY FAN NO. 8

SP-1 -0.24

SP-2 -0.42

SP-3 -0.69

SP-4 5.55





# THOMAS-YOUNG ASSOCIATES

JOB	NAME	HYNES	AUDITORIUM	BOSTON,	MASSACHUSETTS

ADDRESS DATE JUNE 17, 1982

### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-9	S-9			R-9		
LOCATION			Pentho	use			
MANUFACTURE	Americ Standa					American Standard	
MODEL NO.	66800C				1	1-66800-н	
SERIAL NO.	274				490-10	490-10	
SIZE	330				490		
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	30860	27183				14497	
RETURN AIR C.F.M.	0	14497					
O.S.A. C.F.M.	30860	12686					
TOTAL STATIC PRESSURE		7.05				2.57	
SUCTION PRESSURE		-0.95				-1.75"	
DISCHARGE PRESSURE		+6.10"				+0.82"	
MOTOR H.P.	60	60			20	20	
VOLTAGE	480	480			480	480	
PHASE	3	3			3	3	
MOTOR RPM	1775	1775			1770	1770	
FAN R.P.M.	NL	1480			NL	1250	
AMPERAGE	0	46/46/46			2 3	19/19/19	

B.H.P.



#### DUCT TRAVERSE READINGS

SYSTEM S-	9 BRANCH	_A s:	IZE	AREA 2.1	.82 ACT	JAL SP 3.6
			1			
TRAVERSE NO.	1	2	3	4	5	6
1						
	5000					
- 2	4300					
3	4200					
4	4000					
5	4100					
6	4200					
7						
8						
TOTAL	23800					
AVERAGE	3967 -					
TOTAL AV	ERAGE VELO	CITY =	3967	TOTAL CI	M = 8656	

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



Date \_\_ JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S	-9 BRANCH	B SI	ZE	AREA 2	.182 ACT	UAL SP 5.10
TRAVERSE NO.	1	2	3	4	5	6
1	3100					
-2	3100					
3	3100					
4	3200					
5	3200					
6	3300					
7						
8						
TOTAL	19000					
AVERAGE	3167					
TOTAL AV	ERAGE VELO	CITY = 3	167	TOTAL C	FM = _691	0

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

		1		1	1	1
TRAVERSE NO.	1	2	3	4	5	6
1		ļ	<del> </del>	<del> </del>		
	3940			1		
.2	3850					
3	3790					
4	3750					
5	3750					
6	3700					
7	3650					
8	3300					
OTAL	29730					
VERAGE -	3716					

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S-	9 BRANCH	D SI	ZE 20	AREA 2.	182 ACT	JAL SP <u>.93</u>
TRAVERSE NO.	1	2	3	4	5	6
1	1550					
-2	1600					
3	1500					
4	1600					
5	1700					
6	1700					
7						
8						
TOTAL	9650					
AVERAGE	1608					
TOTAL AV	ERAGE VELO	CITY =	1608,	TOTAL CI	M = 350	09-

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' × (W-H) = Sq.Ft.



Date \_\_\_\_\_JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R-	9 BRANCH	A SI	ZE <u>30x22</u>	AREA 4.	58 ACT	UAL SP +.45
TRAVERSE NO.	1	2	3	4	5	6
1						
	700_					
2	700				-	
3	800					
4	800					
5	800					
6	800					
7	800					
8	800					
TOTAL	4600					
AVERAGE	767					
TOTAL AV	ERAGE VELC	CITY =	767	TOTAL CI	2M = 3513	

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft



#### DUCT TRAVERSE READINGS

TRAVERSE NO.	1			ı		
	1					
		2	3	4	5	6
1	1500					ζ.*
	1500					
	1700					į
3	1600					
4	1300					
5	1000					
6	800					
7						
8						
TOTAL 7	7900					-
AVERAGE 1	1317				J. 5	

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{4}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2 + H'' \times (W-H)}{(2)}$  = Sq.Ft.



Date \_\_\_\_JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R.	-9 BRANCH	C SI	ZE 23x24	_ AREA _3	.83 ACT	UAL SP <u>-0.70</u>
TRAVERSE NO.	1	2	3	4	5	6
1	800					
2	850					
3	850					
4	900					
5	900					
6	850					
7	900					
8	1000					
TOTAL	7050					
AVERAGE	881					
AV	ERAGE VELO	CITY =	881	TOTAL CE	M = 3374	_

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' × (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM	R-9 BRANCH	D SI	ZE 19x36	AREA 4	.75 ACT	JAL SP 1.4
TRAVERSE NO.	1	2	3	4	5	6
1	400					`
2	400					
3	400					
4	400					
5	500					
6	500					
7			,			
8						
TOTAL	2600					
AVERAGE	433 ERAGE VELO	CITY -	433	TOTAL CF	'M = 205	

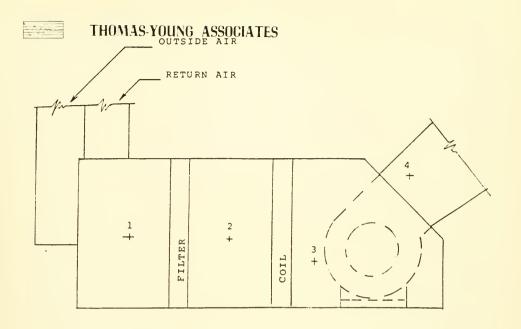
Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

(H")<sup>2</sup> + H" x (W-H) Flat Oval =





UNIT TRAVERSE READINGS

SUPPLY FAN NO. 9

SP-1 -0.45

SP-2 -0.58

SP-3 -.95

SP-4 6.10





# THOMAS-YOUNG ASSOCIATES

JOB NAME	HYNES AUDITORIUM	BOSTON, MASSACHUSETTS
ADDRESS		DATE JUNE 17, 1982

#### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-10				R-10		
LOCATION			Pent	house			
MANUFACTURE	Americ Standa				Americ		
MODEL NO.	66800C				1-6680	00-н	
SERIAL NO.	274				490-14		
SIZE	330				490		
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
TOTAL C.F.M.	33600	26110				18914	
RETURN AIR C.F.M.	5100	18914					
O.S.A. C.F.M.	85000	7196					
TOTAL STATIC PRESSURE		5.5				2.82	
SUCTION PRESSURE		-1.3				-2.75"	
DISCHARGE PRESSURE		4.2				+.07	
MOTOR H.P.	60	60			25	25	
VOLTAGE	480	480			480	480	
PHASE	3	3			3	3	
MOTOR RPM	1775	1,775			1770	1770	
FAN R.P.M.	NL	1390			NL	780	
AMPERAGE	70	38/50/48			27.5	.9/19/19	

B.H.P.

FRAME # 404U

324U



#### DUCT TRAVERSE READINGS

SYSTEM	S-10BRANCH	A SI	ZE _22"	AREA 2.	64ACT	JAL SP 2.6"
TRAVERSE	1	2	3	4	5	6
1	3350					
2	2700					
3	2340					
4	2380					
5	2900					
6	3150					
7	3550					
8	3550					
TOTAL	23920					
AVERAGE	2990					
7	VERAGE VELO	CITY =	2990	TOTAL CH	M = 789	4

Formula for calculation area:

Rectangular Duct =  $W'' \times H'' = Sq.Ft$ .

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $(H'')^2 + H'' \times (W-H)$ 

92



Job Nam THOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM S-	·10 BRANCH	BS:	IZE <u>22"</u>	AREA 2	.64_ ACT	JAL SP 2.15"
TRAVERSE NO.	1	2	3	4	5	6
1	3700					
-2	3450					
3	3300					
4	3200				_	
5	3100					
6	3150					
7	3600					
8	3850					
TOTAL	27350					
AVERAGE	3419					
AVI	ERAGE VELO	CITY =	3419	TOTAL C	FM = <u>9026</u>	

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



## Job Name THOMAS, YOUNG, ASSOCIATES

B GTON, MASSACHUSETTS

Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

		Ī		1	1	
NO.	1	2	3	4	5	6
1	3450					
-2	3350					
3	3250					
4	3300					
5	3450					
6	3550					
7	3650					
8	3850					
TOTAL	27850					
VERAGE	3481					

Formula for calculation area:

Rectangular Duct =  $W'' \times H'' = Sq.Ft$ .

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $(H^*)^2 + H^* \times (W-H)$ (P2) - Sq.Pt



# Job NamTHOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

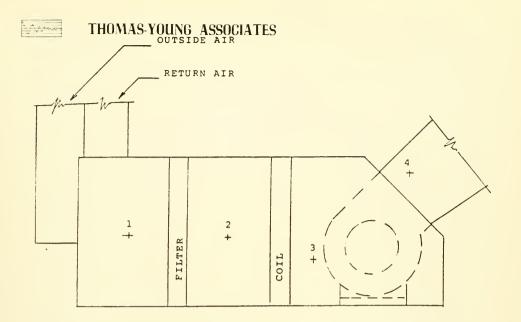
SYSTEM	R-1 OBRANCH	Main SI	ZE <u>28×63</u>	AREA1 22	25ft <sup>2</sup> ACT	JAL SP58
TRAVERSE NO.	1	2	3	4	5	6
1	1200					
-2	1300					
3	1800					
4	1600					
5	1300					
6	1350					
7	1750					
8	2050					
TOTAL	12350					
AVERAGE	1544					
AV	ERAGE VELO	CITY =	1544	TOTAL CI	FM = 1891	`4`

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.





UNIT TRAVERSE READINGS

SUPPLY FAN NO. 10

SP-1 0.70

SP-2-0.75

sp-3 -1.30

SP-4+ 4.2





### THOMAS-YOUNG ASSOCIATES

JOB NAME HYNES AUDITORIUM

ADDRESS BOSTON, MASSACHUSETTS DATE JUNE 23, 1982

#### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	S-11				R-11			
LOCATION	Pentho	use		Penthouse				
MANUFACTURE	Americ			American Standard				
MODEL NO.	1-6680	0 <b>-</b> F			1-6680	00-M		
SERIAL NO.	270=2	74			402-10			
SIZE	270				402			
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL		
TOTAL C.F.M.	23600	18472				14291		
RETURN AIR C.F.M.	18880	*0						
O.S.A. C.F.M.	4720	18472						
TOTAL STATIC PRESSURE		4.56				3.85		
SUCTION PRESSURE		-0.66				-1.50:		
DISCHARGE PRESSURE		3.9				+2.35		
MOTOR H.P.	40	40			20	20		
VOLTAGE	480	480			480	480		
PHASE	3	3			3	3		
MOTOR RPM	1770	1770			1770	1770		
FAN R.P.M.	NL	1620			NL~	960		
AMPERAGE	46	28/26/27			23	20/19/20		

B.H.P.

\*NOTE: Return air damper to S-11 closed



#### DUCT TRAVERSE READINGS

SYSTEM	S-11BRANCH	A SI	ZE _20"	AREA 2	.182 ACT	JAL SP 3.4
TRAVERSE	1	2	3	4	5	6
1	2800					
-2	2300			÷		
3	1750					
4	1700					
5	2200					
6	3000					
7						
8					·	
TOTAL -	13750					
AVERAGE	2292		1202			
AV	ERAGE VELO	CITY =	2292	TOTAL CH	'M = 5	001

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$R^2$$
" = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S-	BRANCH	B S:	IZE	_ AREA _	2.182 ACT	UAL SP 3.
TRAVERSE NO.	1	2	3	4	5	6
1	3000					
·2	3450					
3	2300					
4	2150					
5	2500					
6	2650					
7						
8						
TOTAL	17050		-			
AVERAGE	2842					
AV	ERAGE VELO	CITY =	2842	TOTAL	CFM =6	201

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' × (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM S-11 BRANCH C SIZE 20" AREA 2.182 ACTUAL SP 2.85							
TRAVERSE NO.	1	2	3	4	5	6	
1	3150						
·2	3250						
3	3300						
4	3300						
5	3400						
6	3600						
7							
8	·						
TOTAL	20000						
AVERAGE	3333						
AVERAGE VELOCITY =3333 TOTAL CFM = 7270							

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2 + H'' \times (W-H)}{(2)}$  = Sq.Ft.



# Job Name THO MAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 22, 1982''

#### DUCT TRAVERSE READINGS

SYSTEM R-11 BRANCH Main SIZE 72x31 AREA 15.5 ACTUAL SP 2.45							
TRAVERSE	1	2	3	4	5	6	
1	900	1050	950	1050	1000	700	
. 2	1000	1000	1100	1100	900	600	
3	1000	1000	1050	1150	1000	700	
4	1000	900	1100	1200	1000	6,00	
5	1000	900	1100	1200	1000	500	
6	1000	800	1100	1200	900	400	
7	900	700	1050	1200	900	400	
8	900	700	1000	1000	800	400	
TOTAL	7700	7050	8450	9100	7500	4300	
AVERAGE	962	881	1056	1137	937	560	
AVERAGE VELOCITY = 922 TOTAL CFM = 114291							

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

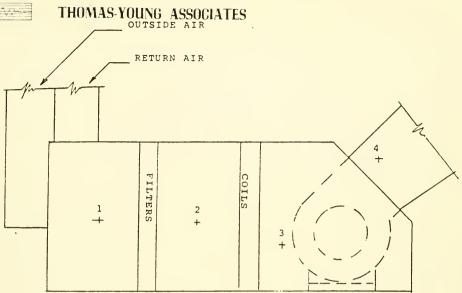
Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.

NOTE: Return air damper to S-11-full-closed







#### UNIT TRAVERSE READINGS

#### SUPPLY FAN NO. 11

SP-1 -0.34

SP-2 -0.41

SP-3 -0.66

SP-4 +3.9





# THOMAS-YOUNG ASSOCIATES

JOB NAME	HYNES AUDITORIUM	BOSTON, MASSAC	HILETTC
ADDRESS		DATE	_

### AIR MOVING EQUIPMENT TEST SHEET

	THE HOVENO DOCTION TEST SHEET							
UNIT NO.	S-12				R-12	R-12		
LOCATION	Appara Room #					Apparatus		
MANUFACTURE	Americ				Ameri	American Standard		
MODEL NO.	1-66800	<b>-</b> G			1-6680	1-66800-N		
SERIAL NO.	330-3	47			365-	365-6		
SIZE	330				365	365		
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL		
TOTAL C.F.M.	17260	12678				14,967		
RETURN AIR C.F.M.	4040	14947						
O.S.A. C.F.M.	13200	0						
TOTAL STATIC PRESSURE		5.36				1.34		
SUCTION PRESSURE		-0.41				-1.40"		
DISCHARGE PRESSURE		4.95				-0.06		
MOTOR H.P.	25	25			10	10		
VOLTAGE	480	480			480	480		
PHASE	3	3			3	3		
MOTOR RPM	1770	1770			1760	1760		
FAN R.P.M.	NL	1280	1.0		NL .	-800		
AMPERAGE	27.5	9/18.5/1	8.5		12	8/7.5/7.5		

B.H.P.



	THOM	AS.Y	OHNG	_ASS	QCIA	TES
me.	**	THES	AUDI	TOKIU	M	

BOSTON, MASSACHUSETTS

Date \_\_\_\_

#### DUCT TRAVERSE READINGS

SYSTEM S	5-12 BRANCH	A SI	ZE	AREA 2.	64 ACT	JAL SP 3.8	
TRAVERSE NO.	1	2	3	4	5	6	
1	1950						
2	2200						
3	2700						
4	2800						
5	2750						
6	2900						
7					-		
8	·						
TOTAL	15300						
AVERAGE	2550						
AVERAGE VELOCITY = 2550 TOTAL CFM = 6732							

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date

#### DUCT TRAVERSE READINGS

SYSTEM S-	12 BRANCH	B SI	ZE	AREA 2.	182 ACT	UAL SP 3.7
TRAVERSE NO.	1	2	3	4	5	6
1	2600					
2	2550	-				
3	2550					
4	2850					
5	2850					
6	2650					
7	2850					
8	2900					
TOTAL	21800					
AVERAGE	2725					

AVERAGE VELOCITY = 2725 TOTAL CFM = 5946

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.



# Job NameTHOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date \_\_\_JUNE 28, 1982

#### DUCT TRAVERSE READINGS

SYSTEM R12 BRANCH Main SIZE 41x28 AREA 7.97ft ACTUAL SP 0									
TRAVERSE NO.	1	2	3	4	5	6			
1	<del> </del>				1				
	1600	1800	1800	2000					
2	1700	1950	2250	2200					
3	1700	2350	2400	2300					
4	1600	2300	2500	2500					
5	1500	2050	2300	2450					
6	1600	1750	1500	1200					
7	1700	1200	1600	800					
8	,•								
TOTAL	11400	13400	14350	13450	e water and	- Adhermany although the account of			
AVERAGE	1628	1914	2050	1921					
VA	ERAGE VELO	CITY =	1878	TOTAL C	FM = 149	67			

Formula for calculation area:

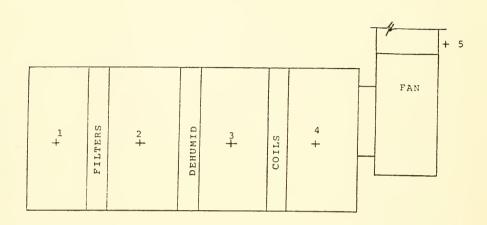
Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



### THOMAS-YOUNG ASSOCIATES



#### UNIT TRAVERSE READINGS

#### - SUPPLY FAN S-12

SP-1 0.05

SP-2 -0.13

SP-3 -0.37

SP-4 -0.41

SP-5 +4.95





### THOMAS-YOUNG ASSOCIATES

JOB	NAME	HYNES	AUDITO	RIUM

BOSTON, MASSACHUSETTS

ADDRESS		

DATE JUNE 17, 1982

#### AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	s-1:	3			R-1:	3
LOCATION	Appara Room 4	tus			Appara Room4	atus
MANUFACTURE	3-2832	3-16			*	
MODEL NO.	6-11-63	3			*	
SERIAL NO.					*	
SIZE	1AB15				*	
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL
TOTAL C.F.M.	4310	3951				2248
RETURN AIR C.F.M.	3370	2248				
0.S.A. C.F.M.	- 940	1703				
TOTAL STATIC PRESSURE		1.13				1.38
SUCTION PRESSURE		-0.20				-1.35
DISCHARGE PRESSURE		+0.93				0.03
MOTOR H.P.	5	5			2	2
VOLTAGE	480	480			480	480
PHASE	3	3			3	3
MOTOR RPM	1725	1725			1740	1740
FAN R.P.M.	NL.	720			NĻ.	1110
AMPERAGE	6	4/4/4			6/3	2/2.5/2.5

B.H.P.

<sup>\*</sup>Not Accessible



### Job Name HOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM 13	B BRANCH	OA SI	ZE 30x16	AREA 3.	3ft <sup>2</sup> ACT	UAL SP - 13
TRAVERSE NO.	1	2	3	4	5	6
1	400	600	700	0	500	
· 2	0	500	750	400	600	
3	0	400	700	400	600	
4	400	500	700	600	7.00	
5	500	600	750	700	900	
6						
7						
8						
TOTAL	1300	2600	3600	2100	3300	
AVERAGE	260	520	720	420	660	
AV	ERAGE VELC	CITY =	516	TOTAL C	FM = 1,70	3

Formula for calculation area:

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)}$$
 + H'' x (W-H) = Sq.Ft.



Date JUNE 17, 1982

#### DUCT TRAVERSE READINGS

SYSTEM _	13 BRANCH	ReturnSI	ZE 12x24	_ AREA _2	ft <sup>2</sup> ACT	UAL SP _	09
TRAVERSE NO.	1	2	3	4	5	6	
1							
	1250	800	1150	1500			
-2	1000	800	1000	1600			
3	900	1000	1200	1150			
4	950	1300	1300	1100			
5							
6							
7							
8							
TOTAL	4100	3900	4650	5350			
AVERAGE	1025	975	1163	1333			
/A	ERAGE VELC	CITY =	1124	TOTAL C	FM = 22	48	

Formula for calculation area:

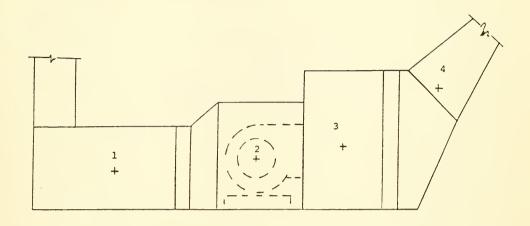
Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval = (H")<sup>2</sup> + H" x (W-H) (2) = Sq.Ft.



### THOMAS-YOUNG ASSOCIATES



#### UNIT TRAVERSE READINGS

#### SUPPLY FAN S-13

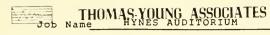
SP-1 -0.13

SP-2 -0.20

SP-3 +0.93

+0.62 SP-4





Address BOSTON, MASSACHUSETTS Date JUNE 28, 1981

#### CIRCULATING WATER PUMP DATA

	1				1	T	T		1	
PUMP	SERV	DESIGN	1	UAL	PD x	AMPS	VOLT	MOTOR	ACTUAL	ВНР
.си		GPM	PRESS		2.31= HD FT	DECTON	PH	DDM	GPM	
		TDH	PSIG	PSIG	HD FT	DESIGN		HP	TDH	
	-		FSIG	PSIG		67.8	480	NR	NR	
1	CW	1200			1					
		120	NR	NR	NR	NR	3	60	NR	
		1200				67.8	480	NR	NR	
2.	CW	120	NR	NR	NR	NR	-3-	60	NR-	
3	CW	2400				112.2	480			
		120	25	63	87.78	87	3	100	87.78	77
	Tower	-								
4	Water	3000				138.31	480	1		
	1	y 117	24	74	115.5	110	3	125	115.5	99
	Tower					67.8	480	NR	NR	
5	Water	227	NR	NR	NR	NR	3	60	NR NR	
	Suppl	у 11/	NK	14 17	MK	1417				
6	Tower	1500				67.8	480	NR	NR	
0	Water		NR	NR	NR	NR	3	60	NR	
	Suppi	7								
										· · ·



# JDB NTHOMAS XQUNG UASSOCIATES

ADDRESS BOSTON, MASS.

DATE 6/30/82

#### DRIVE INFORMATION

	UNIT	FA PULLEY		MOTO		NO. BELTS	FAN RPM	SHEAVE POSITION	C TO C DISTANCE
	S-1	12"	2 15/	16 111	21/2	6	1400	Full Open	56"
	S-2	13½	2 15/	16 11	2 7/8	7	1340	1/2 Open	56"
	s-3	185	2 13/	16 145	2 3/8	6	1380	Full Clsd	57"
	S-4	115	3	11	2 5/8	7	1460	Full Open	58"
	s-5	13½	2 15/	16 11	3	6	1220	Full Open	60
	S-6	13½	2 13/	16 11	2 7/8	6	1200	Full Open	57
S	- 7	14	2 15/	16 10	2 7/8	7	1250	Full Open	60
	S-8	15	3 ½	10	3	6	1060	Full Open	62
	S-9	11	3 5/1	5 10	2 5/8	5	1480	1/2 Open	5 4 "
	S-10	12	2 15/	16 11	2 3/8	6	1,390	Full Open	57
	S-11	10	2 7/1	5 12	2 3/8	4	1620	Full Open	48
	S-12	11	2 5/16	5 9	1 3/8	4	1280	Full Open	55
	S-13	9	1 5/16	7	1 1/8	2	720	1/2 Open	30
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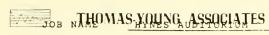
### JOB NTHOMAS HYQUNG JASSOCIATES

ADDRESS BOSTON, MASS. DATE 6/30/82

#### DRIVE INFORMATION

	r		l		1	1	T	
UNIT	FA		мото		NO.	FAN	SHEAVE	C TO C
-	PULLEY	BORE	PULLEY	BORE	BELTS	RPM	POSITION	DISTANCE
R-1	185	2 3/1	6 6	2 1/8	4	620	Full Open	68
R-2	, 25	2 5/1	6 9 ነ	3	4	640	1/2 Open	70
R-3	25	2 7/1	5 11	2 3/8	3	700	Full Open	7 3
R-4	18½	2 5/1	6 9	2 3/8	4	620	Full Open	67
R-5	25	2 3/1	5 9	2	4	640	Full Open	80
R-6	25	2 7/1	5 7	2 5/8	4	540	Full Clsd	70
R-7	15½	2 3/1	5 8	1 3/4	4	830	1/4 Open	56
R-8	18	2 3/1	5 7	2 1/8	4	740	Full Clsd	58
R-9	25	2 5/1	5 9 1/2	1 7/8	3	1250	1/2 Open	7 2
R-10	19	2 5/1	5 9	2 3/8	4	780	Full Open	67
R-11	16	2 3/1	8 12	1 5/8	3	960	Full Clsd	5 4
R-12	131/2	1 13/	16 7	1 1/4	2	800	1/2 Open	50
R-13	6 ½	1 3/1	5 5	5/8	1	1110	Full Open	28





ADDRESS BOSTON, MASS. DATE 6/30/82

#### DRIVE INFORMATION

	Γ		1			-	1	т
UNIT	PULLEY		PULLEY		NO. BELTS	FAN	SHEAVE	C TO C DISTANCE
		DOME	I O D D D D D	DONE		KEH	FOSTITON	DISTANCE
EX-1	153	2	6	13	2	640	Clsd	5 2
EX-2	16	2	5	1 4	2	560	1/2 Open	57
EX-3	15	2 3/1	6 7	14	2	560	Full Open	40
EX-4	13	1 3/1	6 5 1/4	1	None	No B	elt	24
EX-5	19	1 3/1	5 5 ½	7/8	1	256	Full Open	40
EX-6	19	1 ½	5 ½	1 3/	8 1	175	1/2 Open	27½
EX-7	3 ½	15/16	3	1 1/8	3 1	Rng	Full Open	10½
EX-8	3	13/16	3	1	None		elt	101/2
EX-9	3 ½	13/16	3	1 1/8	3 1	Not Rng	1/2 Open	105
EX-10	3 ½	15/16	4	1 1/8	1.	1420	Full Open	101/2
EX-11	3 ½	15/16	4	1 3/8	1	1960	1/2 Open	9 3/4
EX-12	3 ½	15/16	4	1	None	No Be	lt	10
EX-14	4	1 1/8	3 3/4	1 1/8	1	1220	Full Open	131/2
EX-14	13	1 13/1	.6	14	2	730	Full Open	5 5
EX-15	NOT	TESTED			Window Prop			
EX-16	NOT	rested			Window Prop			
EX-17	8 7	1 3/8	4 ½	3/4	1	920	Closed	33
EX-18	3 ½	15/16	3 ½	1 3/8	1 F	Not Lunning	Full Clsd	9 3/4



ADDRESS BOSTON, MASS.

DATE 6/30/82

#### SUPPLY AIR FAN

#### TEMPERATURE INFORMATION

UNIT	SUPPLY AIR TEMP.	RETURN AIR TEMP.	MIXED AIR TEMP.	OUTSIDE AIR TEMP.
S-1	55.4	70.5	73.4	7 4
S-2	5 8	70.6	73.4	7 4
S - 3	64.9	73.8	75.6	74
5 - 4	56.2	70.0	72.1	74
s - 5	51.1	67	68.9	74
s-6	56.7	68.8	72.5	74
s-7	54.6	70.6	70.27	74
S-8	54.8	75.9	76.3	74
S-9	52.8	70.5	70.6	74
S-10	49.3	68.9	72.3	74
S-11	52.2	68.5	70.3	74
S-12	55	69.4	69.4	77.5
S-13	58	67	74	77.5





# THOMAS YOUNG ASSOCIATES

Address BOSTON, MASSACHUSETTS Date JUNE 30, 1982

EX-1	EX-2	EX-3	EX-4	EX-5	EX-6	EX-7
Am Std	Am Std	Am Std	Am Std	No Name	Am Std	No Name
445	402		1118	plate	2L20	plate
App 2	App 2	Food Concess Storage	Gen Rm	Boiler Rm	Boiler Rm	Pent house
1.15	1.15	1.15	1.15	1.25	1.15	No Name- plate
480/3	480/3	480/3	480/3	220/480	480/3	
9.2	6.4	1.2	3.85	3.6/1.8	6.0	
8.0/8.0	4.0/4.0	7.5/6.5 6.5	2.4/2.3	1/1/	1.5/1.5	Not Running
640	560	560	No	256	175	
Clsd	1/2 Open	Full Open	Belts	Full Open	Open	Full Open
See Dwgs.	See Dwgs.	See Dwgs.	See Dwgs	See Dwgs	See Dwgs	See Dwgs
14,000	12,788	12,160	1	2091	No acces to ducts	sNot Running
7.5	5	10	3	1	5	
2.31	1.73	1.18	Not	1.01	.07	NR
2.10"	-1.3	-0.75	On	-0.61	.01	NR
.21"	+0.43	-0.43	1	0.40	.06	NR
	Am Std  445  App 2  1.15  480/3  9.2  8.0/8.0  8.0   640  Clsd See Dwgs.  14,000  7.5   2.31  2.10"	Am Std Am Std  445 402  App 2  1.15 1.15  480/3 480/3  9.2 6.4  8.0/8.0 4.0/4.0  8.0 4.0  640 560  Clsd 0pen See Dwgs.  14,000 12,788  7.5 5  2.31 1.73  2.10" -1.3	Am Std Am Std Am Std  445 402  App 2 2 Storage  1.15 1.15 1.15  480/3 480/3 480/3  9.2 6.4 1.2  8.0/8.0 4.0/4.0/.5/6.5  8.0 4.0 6.5   640 560 560  Clsd 0/2 Full Open See See Dwgs. Dwgs.  14,000 12,788 12,160  7.5 5 10   2.31 1.73 1.18  2.10" -1.3 -0.75	Am Std Am Std Am Std Am Std  445 402 1L18  Appp 2 Concess Rm  1.15 1.15 1.15 1.15  480/3 480/3 480/3 480/3  9.2 6.4 1.2 3.85  8.0 4.0 6.5 2.4/2.3  8.0 4.0 6.5 2.4/2.3  8.0 560 560 No  Clsd 0560 560 No  Clsd 0pen 0pen Belts  See Dwgs. Dwgs. Dwgs  14,000 12,788 12,160 1  7.5 5 10 3   2.31 1.73 1.18 Not  2.10" -1.3 -0.75 On	Am Std Am Std Am Std Am Std No Name  445	Am Std Am Std Am Std Am Std No Name Am Std  445





## TOD Name THOMAS YOUNG ASSOCIATES

Address BOSTON, MASSACHUSETTS Date JUNE 30, 1982

		,					
FAN NO.	EX-8	EX-9	EX-10	EX-11	EX-12	EX-13	EX-14
MFG.	Am Std	Am Std	Am Std	Am Std	No Nmplt	Am Std	Am Std
SIZE	122	12285	122	135		165EW	165
LOCATION	Pent house	Pent house	Pent house	Pent house	Pent house	Pent house	Pent house
SAFETY FACTOR	No Nmplt	1.35	1.0	1.25	No Nmplt	No Nmplt	NL
VOLT./ PH	Needs Belt	115/1	440/3	440/3		11	480/3
AMP RATING	Not Running	4.4		2.6/1.3	n	11	6.4
ACTUAL AMPS	.,	NR_	1.0/1.0	1.4/1.3	11	1.8/1.8	4.6/4.6
DESIGN RPM (FAN)	"	NR			NL		
ACTUAL RPM (FAN)	"	NR	1420	1900	NR	1400	1720
POSITION	n	1/2	Open	Clsd		Open	Open
REQUIRED CFM	11						
ACTUAL CFM	"		692	1300	No Belt	2640	4576
Н.Р.	11		1/2	3/4	"		5
DESIGN SP	D		NL	NL	NL	NL	NL
ACTUAL SP	н		. 73	-2.23	-	1.33	2:44
SUCTION SP			63	-2.0		-1.1	-2.4
DISC. SP.			+.10	.23		. 2 3	.04



# THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM

b	Name	HYNES	AUDITORIUM

Address BOSTON, MASSACHUSETTS Date JUNE 30, 1982

FAN NO.	EX-15	EX-16	EX-17	EX-18		
MFG.	Am Std	Am Std	Am Std	Am Sto	a l	
SIZE	24CT	24CT	245	122B5		
LOCATION	Pent house	Pent house	APP 2	Pent house		
SAFETY FACTOR			1.20	NL		
VOLT./ PH 1	G Ei	Q	208/220 480/3	115/230		
AMP RATING	ST	ST	5/2.5	5.2/2.	6	
ACTUAL AMPS	TE	T 2	2.4	WE		
DESIGN RPM (FAN)			920	COULD		
ACTUAL RPM (FAN)			Open	NOT		
SHEAVE POSITION	NOT	NO.		OPERATE		
REQUIRED CFM				THIS		
ACTUAL CFM	Window Prop	Window Prop	4054	UNIT		
н.Р.			1 1/2			
DESIGN SP			かし			
ACTUAL SP			1.62			
SUCTION SP			-0.32			
DISC. SP.			+1.3"			





# THOMAS-YOUNG ASSOCIATES Job Name HYNES AUDITORIUM

Address BOSTON, MASSACHUSETTS Date JULY 1, 1982

FAN NO.	V-1	V <b>-</b> 2	V-3	V-4	v <b>-</b> 5	V-6	V-7
MFG.	Am Std	Am Sto	Am Std	There	Am Std	Am Std	Am Std
SIZE	NA	NA	NA	is	1L15	N A	109
LOCATION	Shop	Shop	Shop	No	Area	Area	house
SAFETY FACTOR	1.15	1.15	1.15	V-4	1.25	1.15	1.25
VOLT./ PH	480/3	80/3	480/3		220/440	480/3	440/3
AMP RATING	9.2	9.2	9.2		3.4/1.7	9.2	1.9/.95
ACTUAL AMPS	4.6/4.8	4.6/4.2	3.6/3.4		1.0/1.0	3.8/4.0	.5/.5
DESIGN RPM (FAN)						NL	
ACTUAL RPM (FAN)	650	NA	NA		650	620	1100
SHEAVE POSITION	Full Open	80% Open	80% Open		Full Open	7/8 Clsd.	1/2
REQUIRED CFM						NL	
ACTUAL CFM	19153	14644	15000		2910	9190	549
Н.Р.	7.5	7.5	7.5		1	7.5	1/2
DESIGN SP	NL	NL	NL	===	NL	NL	NL -
ACTUAL SP	0.62	0.90	0.64		0.14	0.64	0.40
SUCTION SP	-0.42	-0.45	-0.05		-0.13	-0.41	02
DISC. SP.	0.2	0.45	0.59		.01	0.23	.38



Address	BOSTON, MASSACHUSETTS	Date JULY 1, 1982

FAN NO.	V-8	V <b>-</b> 9		·	
MFG.	Am Std	Am Std			
SIZE	1V9	1V9			
LOCATION	Pent house	Pent house			
SAFETY FACTOR	1.25	1.25			
VOLT./	440/3	440/3			
AMP RATING	1	1.9/.95			
ACTUAL AMPS	.8/.8	.5/.5			
DESIGN RPM (FAN)					
ACTUAL RPM (FAN)	322	346			
SHEAVE POSITION	Open	Open			
REQUIRED CFM	Check Dwgs.	Check Dwgs.			
ACTUAL CFM	656	847			
н.Р.	1/2	1/2			
DESIGN SP	NL	ЙL ¯			
ACTUAL SP	.07	.08			
SUCTION SP	.07	.05			
DISC. SP.	0.00	.03			



### NamTHOMASYQUEGOASSOCIATES BOSTON, MASSACHUSETTS

Date JULY 1, 1982

#### DUCT TRAVERSE READINGS

SYSTEM E	-1 BRANCH	Main SI	ZE <u>45×40</u>	_ AREA _1	25 ACT	UAL SP +0.44
TRAVERSE NO.	1	2	3	4	5	6
1						
	1200	1300	1150	800		
· 2	1200	1250	900	800		
3	1200	1250	900	850		
4	1200	1250	900	950		
5	1200	1250	1000	1000		
6	1300	1300	1050	1050		
7	1300	1300	1100	1050		
8	1350	1300	1150	1050		
TOTAL	9950	10200	8150	7550		
AVERAGE	1244	1275	1019	944		
AV	ERAGE VELC	CITY =	1120	TOTAL C	FM = 140	000

Formula for calculation area:

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM E	-2 BRANCH	SI	ZE 50x36	AREA 1	2.5 ACT	UAL SP	-1.3
	1	1	1	1	T	1	
TRAVERSE NO.	1	2	3	. 4	5	6	
1	1100	1050	1150	1500	1100		
-2	1100	1100	1100	1150	1000		
3	1100	1050	1050	1200	1000		
4	1100	1000	900	1000	1000		
5	1000	900	800	1000	900		
6	1000	800	800	850	900		
7							
8							
TOTAL	6400	5900	5800	6700	5900		
AVERAGE	1067	983	967	1117	983		
AV	ERAGE VELC	CITY =	1023	TOTAL C	FM = 127	88	

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)}{(2)} = Sq.Ft.$$





# Job Nam THOMAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JULY 2, 1982

### DUCT TRAVERSE READINGS

SYSTEM E-	-3 BRANCH	Disch.SI	ZE <u>80x23</u>	AREA 12	2.8 ACT	UAL SP +.43
	,				<del>,</del>	<del> </del>
TRAVERSE NO.	1	2	3	4	5	6
1	1050	900	1000	00	800	
-2	1000	900	1000	900	900	
3	1100	900	1000	900	900	
4	1000	900	1000	950	900	
5	1000	900	1000	950	900	
6	1000	900	1000	950	950	
7	1000	900	1000	950	950	
8						
TOTAL	7150	6300	7000	6500	6300	
AVERAGE	1021	900	1000	929	900	
AVERAGE VELOCITY = 950 TOTAL CFM = 12160						

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



Date \_\_\_JULY 1, 1982

### DUCT TRAVERSE READINGS

SYSTEM E	X-5 BRANCE	· SI	ZE <u>38×14</u>	_ AREA 3	7ft <sup>2</sup> ACT	UAL SP +0.40
TRAVERSE	1	2	3.	4	5	6
1	600	500	600	600	600	
-2	600	500	600	500	700	
3	600	500	500	500	650	
4	600	500	500	500	650	
5						
6						
7						
8						
TOTAL						
AVERAGE	600	500	550	5 2 5	650	
AVI	ERAGE VELO	CITY =	565	TOTAL C	FM = 2091	

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



### DUCT TRAVERSE READINGS

SYSTEM E-	-17 BRANCH	SI	ZE 2 <u>6½x19½</u>	AREA 3.	59 ACT	UAL SP +1.45
TRAVERSE NO.	1	2	3	4	5	6
1	900	1100	1300	1300	1400	
-2	1000	1100	1250	1300	1400	
3	1000	1000	1200	1200	1300	
4	1000	1000	1200	1000	1200	
5	000	1000	1200	700	1100	
6						
7						
8						
TOTAL						
AVERAGE	980	1040	1230	1100	1280	
AVE	ERAGE VELC	CITY =	1126	TOTAL C	FM = 4054	1

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



# JOB NATHOMASHYOLINGUASSOCIATES

A			

BOSTON, MASS.

DATE 6/30/82

## DRIVE INFORMATION

	·r	. –	1 -					
UNIT	FA PULLEY		MOTO		NO. BELTS	FAN	SHEAVE POSITION	C TO C DISTANCE
V-1	13"	1 3/1	6 5 1/4	7/8	1	650	Full Open	20"
V - 2	27"	2 5/1	6 8"	1 3/8	2	NA	80% Open	3 2 "
V-3	27"	2 5/1	6 8"	1 3/8	2	NA	80% Open	32"
V-4			No	V-4	1	:		
V = 5	18"	1 5/8	6 1/2	1 5/8	2	640	7/8 Clsd	29"
V-6	16"	1 9/1	6 6 "	1 5/8'	2	620	7/8 Clsd	30"
V - 7	7"	1 3/1	5 5"	7/8"	1	1100	1/2 Open	12"
V-8	5½"	1 3/16	5 5"	NA	1	322	Full Open	22½"
V-9	7"	13/16	5 5 "	7/8"	1	346	Full Open	12"
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### DUCT TRAVERSE READINGS

SYSTEM	V-1 BRANCE	S S	ZE 18x23	_ AREA 17	.9ft <sup>2</sup> ACT	UAL SP 0.4
TRAVERSE NO.	1.	2	3	4	5	6
1	1500	1600	1200	700	500	
·2	1500	1700	1100	700	500	
3	1600	1700	1000	700	500	
4	1500	1500	1000	700	500	
1500	1500	1400	1000	800	500	
6	1500	1400	1100	700	500	
7	550	1800				
8						
OTAL	10650	10800	6400	4300	3000	
VERAGE	1521	1543	1067	717	500	

Formula for calculation area:

Rectangular Duct =  $\frac{W" \times H"}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)}$$
 = Sq.Ft.





# Name THO MAS YOUNG ASSOCIATES BOSTON, MASSACHUSETTS

Date JULY 1, 1982

#### DUCT TRAVERSE READINGS

SYSTEM V	-2 BRANCE	Discharge	ZE 65x26	_ AREA <u>11</u>	.8ft <sup>2</sup> ACT	UAL SP +0.2
TRAVERSE NO.	1	2	3	4	5	6.
1		-		-		
1	1150	1200	1150	1100	1000	
· 2	1050	1200	1200	1200	1150	
3	1100	1200	1300	1250	1200	
4	1200	1200	1300	1300	1250	
5	1250	1200	1300	1300	1200	
6	1200	1150	1250	1300	1200	
7	1200	1100	1200	1300	1200	
8				1200	1200	
TOTAL	8150	8250	8700	9950	9400	
AVERAGE	1164	1178	1443	1244	1175	
AV	ERAGE VELO	CITY =	1241	TOTAL C	FM = 146	544

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval =  $\frac{(H'')^2}{(2)}$  + H'' x (W-H) = Sq.Ft.



#### DUCT TRAVERSE READINGS

SYSTEM	V-3BRANCE	SuctionSI	ZE 72×40	AREA 201	t 2 ACT	UAL SP -0.05
TRAVERS NO.	E . 1	2	3	4	5	6
1						
	600	800	700	800	600	
2	700	900	700	900	600	
3	600	800	750	800	700	
4	700	900	700	850	700	
5	800	800	800	800	700	
6	700	800	750	850	700	
7						
8						
TOTAL	4100	5000	4400	5000	4000	
AVERAGE	683	833	733	833	667	
	AVERAGE VELO	OCITY =	750	TOTAL C	FM = 1500	0.0

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{R^2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



#### DUCT TRAVERSE READINGS

TRAVERSE NO.	1	2	3	4		
			İ		5 .	6
1 7	700					
.2 8	800					
3 8	300					
4 7	700					
5 7	700					
6 8	300					
	50					
8						
TOTAL						
AVERAGE			750	TOTAL C	FM = 29	

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2 + H'' \times (W-H)}{(2)} = Sq.Ft.$$



Date \_\_\_JULY 1, 1982

#### DUCT TRAVERSE READINGS

SYSTEM	-6 BRANCH	SI	ZE 24x60	AREA 10	ft 2 ACTU	JAL SP <u>+0.2</u> 3
TRAVERSE NO.	1	2	3	4	5	6
1	1100	1000	800			
·2	1100	1000	800			
3	1150	900	900			
4	1100	1100	900			
5	1050	1000	900			
6	1000	1000	800			
7	800	800	700			
8 .						
TOTAL	7400	6800	5800			
AVERAGE	1057	971	729			
AV	ERAGE VELC	CITY =	919	TOTAL C	FM = 919	0

Rectangular Duct = 
$$\frac{W" \times H"}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.



THOMAS YOUNG ASSOCIATED
-------------------------

ADDRESS	BOSTON,	MASS.	DATE	6/30/82	

# DRIVE INFORMATION

	r							
UNIT	FA		MOTO		NO.	FAN	SHEAVE	СТОС
	PULLEY	BORE	PULLEY	BORE	BELTS	RPM	POSITION	DISTANCE
WCV-1		No E	Belts		Not Rng	1		Enclosed
		, NO I				-	1	Direct Drive
2			No	Ac	cess			
3			Dire	ct Dr	ive			
. 4	4 3	1 3/16	5 4	14	None	<u>:</u>		14
5	6	11/16	6	1 1/8	1	1560	1/2 Open	26
6	5 ½	1 3/16	4	1 1/8	1	1080	Full Open	13 3/4
7	Not	Running	g (Encl	osed U	nit)			
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# THOMAS-YOUNG ASSOCIATES

JOB NAME HYNES AUDITORIUM

ADDRESS BOSTON, MASSACHUSETTS DATE JULY 1, 1982

# AIR MOVING EQUIPMENT TEST SHEET

UNIT NO.	WCV-1		WCV-	2	WCV-3	3
LOCATION			Column I-150 Basement		Boiler Room	
MANUFACTURER	<del>                                     </del>		Opp Ele	Opp Elevator		:d
MODEL NO.	10SHR					
SERIAL NO.	NA					
·SIZE	•				75M	
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL
TOTAL C.F.M.	Needs			NO	NL	963
RETURN AIR C.F.M.	Belt			A	NL	963
O.S.A. C.F.M.				С	NL	0
TOTAL STATIC				С	NL	0.34
SUCTION PRESSURE				E	NL	-0.03
DISCHARGE PRESSURE		Not		S	NL	0.31
MOTOR H.P.	1/4	Running		S	NL	1/6 -
VOLTAGE	480				NL	1/5
PHASE	1				NL	1
MOTOR RPM	1750				NL	1140
FAN R.P.M.					- 1	Direct Drive
AMPERAGE	4.4				4	2





# THOMAS-YOUNG ASSOCIATES

JOB NAME HYNES AUDITORIUM

3.8/1.8

AMPERAGE

ADDRESS BOSTON, MASSACHUSETTS DATE JULY 1, 1982

### AIR MOVING EQUIPMENT TEST SHEET

	UNIT NO.	WCV-	4	WCV-	WCV-5		WCV-6	
	LOCATION	Penthor	Penthouse		Penthouse		Penthouse	
	MANUFACTURE	Am Std		Am St	Am Std		:d	
	MODEL NO.	1651	P	182	182			
	SERIAL NO.	н1651	) V 2	SER	81			
	•							
	OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	
	TOTAL C.F.M.		,	NL	1855		3994	
	RETURN AIR C.F.M.		NO	NL	1855		3994	
	O.S.A. C.F.M.		В	NL	0		0	
	TOTAL STATIC PRESSURE		E	NL	1.24		0.80	
	SUCTION PRESSURE		L	NL	0.35		76	
	DISCHARGE PRESSURE		т	NL	0.87		+.04	
	MOTOR H.P.	1	1	NL	2		1	
_	VOLTAGE	40/480	240/480 2	40/480	240/480	240/480	240/480	
_	PHASE	3	3	3	3	3	3	
	MOTOR RPM	1730	1730	1750	1750	1730	1730	
	FAN R.P.M.	NL	NR	NL	1560	NL	1247	

7.2/3.6 3.1 3.6/1.8

1.6/1.7/



### DUCT TRAVERSE READINGS

SYSTEM WCV-3BRANCH SIZE 10x10 AREA 0.69 ACTUAL SP +.29						
		i i	1	1		1
TRAVERSE NO.	1	2	3 .	4	5	6
1	1700	1900				
-2	1900	1850				
3	1850	1850				
4	1890	1800				
5						
6						
7						
8						
TOTAL						
AVERAGE	1813	1850				
AUPPACE UPLOCITY - 2002 TOTAL CEM = 1002						

AVERAGE VELOCITY = 1831 TOTAL CFM = 1263

Formula for calculation area:

Rectangular Duct =  $\frac{W'' \times H''}{144}$  = Sq.Ft.

Round Duct =  $\frac{2}{144}$  = Sq.Ft.



# Job NameTHOMASYOUNGOASSOCIATES BOSTON, MASSACHUSETTS

Date JULY 2, 1982

### DUCT TRAVERSE READINGS

SYSTEMW	CV-5BRANCE	Suctions	ZE 26x12	AREA 2.	16 ACT	UAL SP
TRAVERSE NO.	1	2	3	4	5	6
1	900	900	900			
2	900	900	900			
3	900	1000	900			
4	900	900	900			
5	900	800	800			
6	800	800	800			
7	800	750	700			
8						
TOTAL	6100	6050	5900			
AVERAGE	871	864	843			
AV	ERAGE VELO	CITY =	859	TOTAL C	FM = 185	5 5

Rectangular Duct = 
$$\frac{W'' \times H''}{144}$$
 = Sq.Ft.

Round Duct = 
$$\frac{R^2}{144}$$
 = Sq.Ft.

Flat Oval = 
$$\frac{(H'')^2}{(2)} + H'' \times (W-H)$$
 = Sq.Ft.





# THOMAS-YOUNG ASSOCIATES

3.6/1.8

NR

AMPERAGE

7.

JOB NAME	HYNES AUDITORIUM	BOSTON,	MASSACHUSETTS
ADDRESS		DATE JULY 1, 198	32

	AIR	MOVING E	QUIPMENT	TEST SH	EET	
UNIT NO.	WC	v <b>-</b> 7				
LOCATION	Penti	nouse				
MANUFACTURE	R Am Sto	i				
MODEL NO.	150					
SERIAL NO.						
OPERATING CONDITIONS	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL	SPECI- FIED	ACTUAL
TOTAL C.F.M.		NO				
RETURN AIR C.F.M.		В				
0.S.A. C.F.M.		E				
TOTAL STATIC PRESSURE		L				
SUCTION PRESSURE		т				
DISCHARGE PRESSURE						
MOTOR H.P.	1	1				
VOLTAGE	240/480	240/480			i	
PHASE	3	3				
MOTOR RPM	1730	NR				
FAN R.P.M.	NL	NR				



Support Documentation

Plumbing

Robert W. Sullivan Inc.



# HYNES AUDITORIUM EXPANSION

# Plumbing and Fire Protection

# VOLUME II (SUPPORTING DOCUMENTATION)

# INDEX

Paragraph Number	Paragraph Title	Page No.
Α.	UTILITIES	1
	<ol> <li>Cold Water Supply</li> <li>Storm Drainage</li> <li>Sanitary Sewers</li> </ol>	1 1 2
В.	EQUIPMENT	2
	<ol> <li>Domestic Water Pump</li> <li>Sewage Ejector</li> <li>Fire Pump</li> <li>Domestic Hot Water Heater and Air Compressor</li> </ol>	2 2 2 2



### A. UTILITIES

### 1. COLD WATER SUPPLY

Hydrant flow tests were conducted for the above project on June 4, 1982, the following are the locations and the results:

a. Dalton Street and Scotia Street for Low Service at fire hydrant No. 1

Static Pressure Residual Pressure		psi psi
Flow	1980	gpm
GPM Available @ 20		
psi	4190	gpm

b. Boylston Street between Fairfield Street and Hereford Street for High Service at fire hydrant No. 2.

Static Pressure Residual Pressure	74	psi psi
Flow GPM Available @ 20	1980	gpm
psi	3940	qpm

c. Gloucester Street between Newbury Street and Boylston Street for Low Service at fire hydrant No. 3.

Static Pressure	60	psi
Residual Pressure	48	psi
Flow	3220	qpm
GPM Available @ 20		
psi	6200	gpm

These results indicate an adequate water supply for both domestic and fire protection purposes.

Refer to attached sketch showing the location of fire hydrants.

## 2. STORM DRAINAGE

The drainage piping collect surface water and building conductors and discharges to the following storm drains in the street:

	Street Name	Size of Pipe in Inches	Roof Area in Square Feet
a.	Boylston	8	8,100
b.	Boylston	15	46,297
С.	Dalton	12	26,325
d.	Dalton	15	52,313
		Total	133,034 sq/ft



The following are the two land areas for the expansion on Ring Road:

-	Hynes Audit Prudential	Company		11,360 11,436	17
			Total	2,796	sq/ft

The storm drainage for the roof of the new expansion which is equal to the area of Ring Road will drain in the same piping draining Ring Road.

### SANITARY SEWERS

The sanitary sewers from the building collect and discharge to the following main sewers in the street:

	Street Name	Size of Pipe in Inches	Maximum Load in in Fixture Units
a.	Boylston	8	2100
b.	Boylston	8	2100
С.	Dalton	10	3750

The sanitary sewers for the new expansion will be determined in the next phase.

### B. EQUIPMENT

The following are Preliminary sizes for the equipment required for the new expansion:

### 1. DOMESTIC WATER PUMP

Domestic water pump shall be duplex unit, each pump capacity is 400 GPM, boosting the pressure 85 PSI, 10 H.P.

### SEWAGE EJECTOR

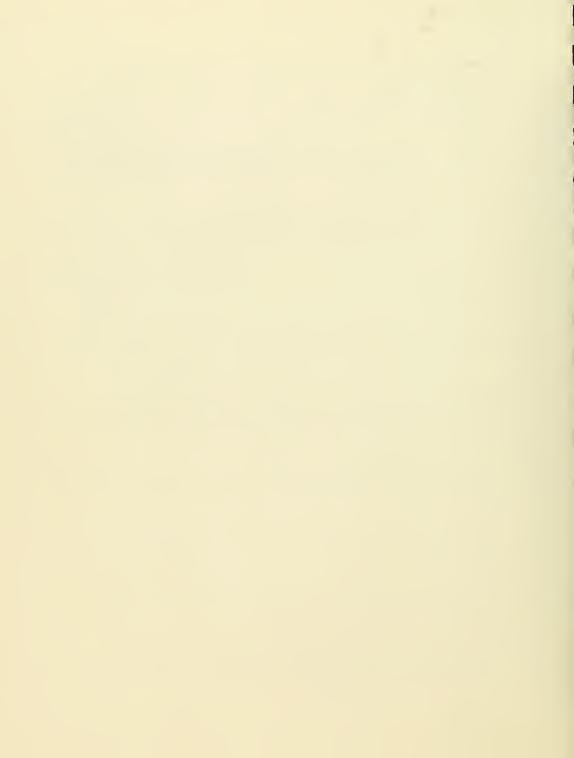
Sewage ejector shall be duplex unit, each pump capacity is 200 GPM @ 30' head, 3 HP.

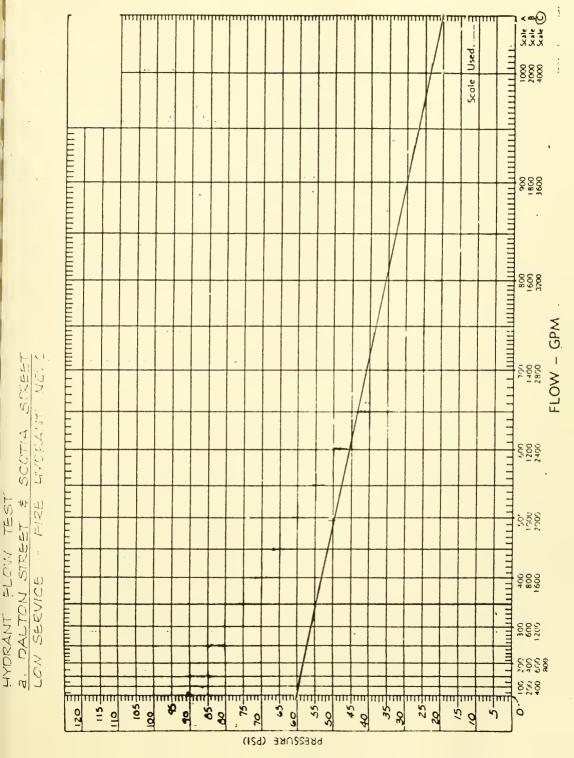
### 3. FIRE PUMP

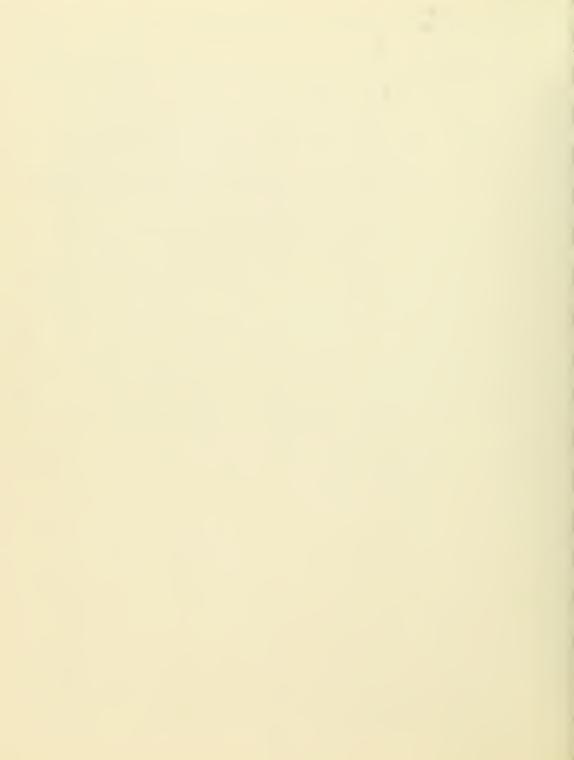
Fire pump shall be 2500 GPM, boosting the pressure 120 PSI, 200 HP. Jockey pump shall be 5 HP.

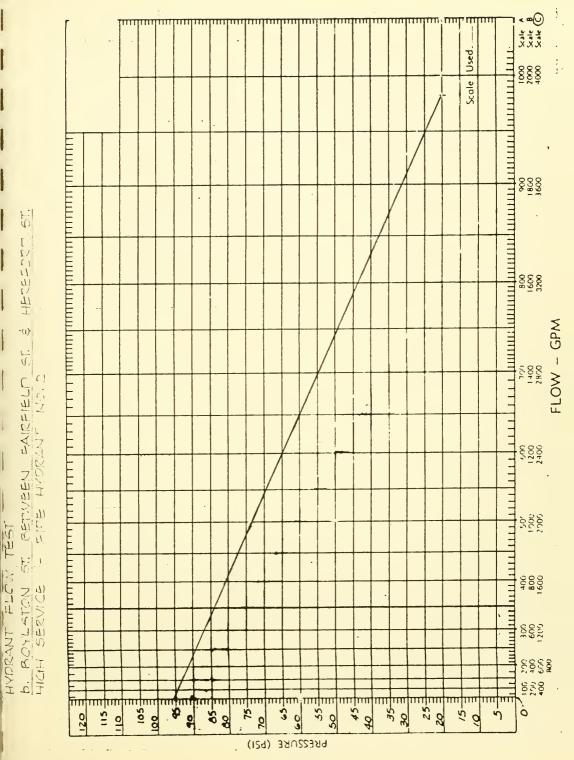
### 4. DOMESTIC HOT WATER HEATER AND AIR COMPRESSORS

Domestic hot water heaters, circulating pumps, air compressors and air receivers shall be determined in the next phase.

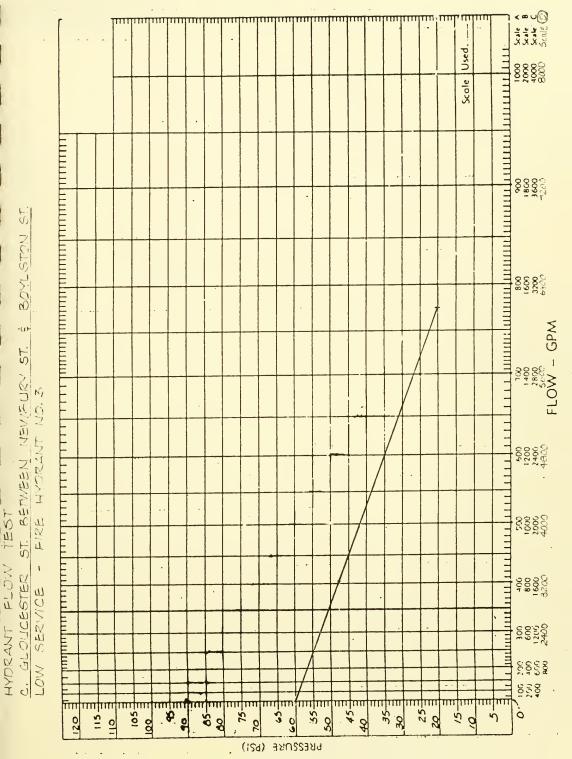




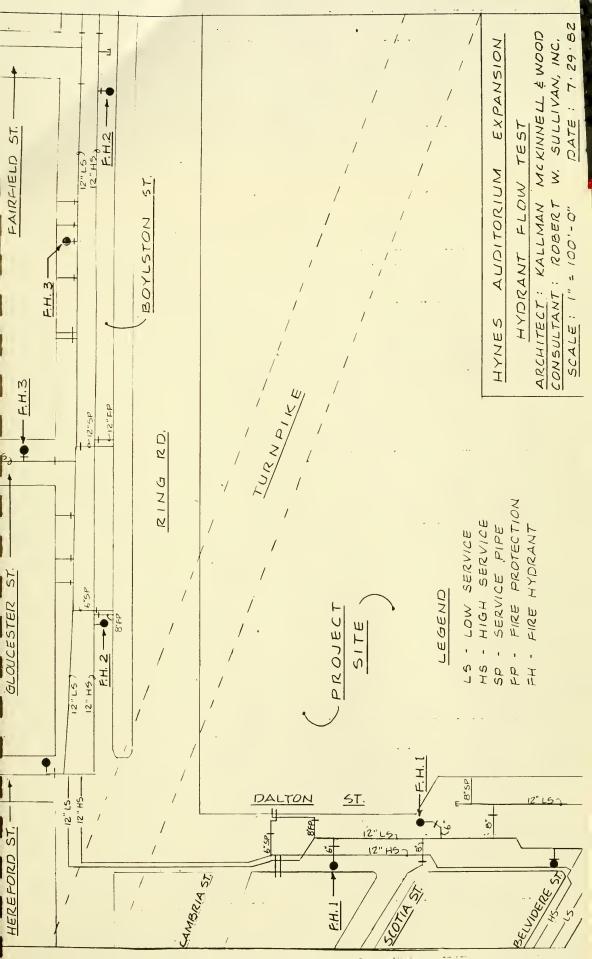














# Support Documentation

Electrical

Lottero & Mason Associates, Inc.





Consulting Engineers 132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367

January 7, 1983

Principals

ALFRED E LOTTERO PE
PRESIDENT

JOHN D. DE VEUVE PE
LITE PRESIDENT

DUIS A PERCOLO PE
LICE PRESIDENT

Associates

RULINAM J. HENNEY
RULIN A. MARAMALDE PE
BRIAN M. MCCORMACK

Boston Edison Company 800 Boylston Street, PB4 Boston, Massachusetts 02199

ATTENTION: Mr. James M. Russell

RE: Hynes Auditorium Expansion Boston, Massachusetts #0305-1-82

#### Gentlemen:

This is to confirm our understanding of numerous telephone conversations we have had over the past few months, and our discussion at a meeting in this office on January 4, 1983 regarding the expansion of the Hynes Auditorium.

- The existing basement transformer vault on the Dalton Street side of the facility which presently contains four 1000 KVA, 13.8 KV to 277/480 volt, 3¢ transformers is of sufficient size to accommodate an increase in transformation to four 2000 KVA transformers without altering the physical characteristics of the room. This has been confirmed by Boston Edison Co. field engineering.
- 2. Underground 13.8 KV primary service is available from Boylston Street to serve a new transformer vault on the lower basement level in the north-eastern corner of the new addition to the building.
- 3. The peak maximum demand of the existing facility was 2124 KW recorded in June of 1981.

As you are aware, the HVAC system being proposed under the expansion program is unresolved. An energy study will be undertaken in the next phase of design work by the mechanical engineering discipline to ascertain the most efficient and economical HVAC system. At the completion of that study, and following a decision by the Owner, a breakdown of the preliminary electrical loads will be forwarded to you for your evaluation of transformation needed to serve the renovated existing and new structures.

Thank you for your assistance.

Very truly yours,

LOTTERO & MASON ASSOCIATES, INC.

Brian M. McCormack





Consulting Engineers 132 LINCOLN STREET

BOSTON, MA 02111 (617) 423-7367

January 7, 1983

Principals

ALFRED E LOTTERO PE
PPESIDENT
JOHN D DE VEUVE PE
VICE PRESIDENT
LOUIS A PERCOCO PE
VICE PRESIDENT

Associates

WILLIAM I HENNEY

RUDY A MARAMALD, PE

BRIAN M. MCCORMACK

New England Telephone Company Building Industry Consulting Service 245 State Street - Room 501 Boston, Massachusetts 02109

ATTENTION: Mr. Harold L. Dolan

RE: Hynes Auditorium Expansion Boston, Massachusetts #0305-1-82

### Gentlemen:

This is to confirm my understanding of items discussed at our meeting in this office on January 6, 1983 concerning the proposed expansion program at the Hynes Auditorium.

- 1. N.E.T.Co. feels the existing four 4-inch underground service conduits from Dalton Street are sufficient to serve the 375,000 square foot expansion program of the facility.
- The existing basement main telephone equipment frame room may need to be expanded. N.E.T.Co. field engineers will investigate and inform this office of their decision.
- 3. Underground telephone service is not available from Boylston Street.

We will be forwarding to you in the next phase of design work detailed information regarding interior communication requirements.

Thank you for your assistance.

Very truly yours,

LOTTERO & MASON ASSOCIATES, INC.

Brian M. M. Cormack
Brian M. McCormack

BMM:n





132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367

January 3, 1983

Principals

ALFRED E LOTTEPO, PE
PRESIDENT
JOHN D DE VEUVE PE
VICE PRESIDENT
LOUIS A PERCOCO PE
VICE PRESIDENT

Associates

WILLIAM J. HENNEY
RUDY A. MARAMALDI PE
BRIAN M. MCCORMACE

Boston Fire Department Fire Alarm Division P. O. Box 218 Astor Station Boston, Massachusetts 02110

ATTENTION: Superintendent John Murphy

RE: Hynes Auditorium Expansion
Boston, Massachusetts
#0305-1-82

Dear Superintendent Murphy:

This is to confirm our telephone conversation of November 10, 1982 concerning the proposed expansion of the Hynes Auditorium.

As discussed, the existing facility is connected to the city's municipal fire alarm circuit through an existing master box within the building. Under the expansion program, this connection is to be maintained.

Also, as you mentioned, the existing interior fire alarm system is quite minimal and under an expansion program of this magnitude, will need to be brought up to current fire safety standards for a building of this type in accordance with the Mass. State Building Code.

Thank you for your assistance.

Very truly yours,

LOTTERO & MASON ASSOCIATES, INC.

Brig M. M. Yomed

Brian M. McCormack

BMM:n





132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367 Principals

ALFRED E LOTTERO PE PRESIDENT

JOHN D DE VEUVE PE VICE PRESIDENT

LOUIS A PERCOCO, PE VICE PRESIDENT

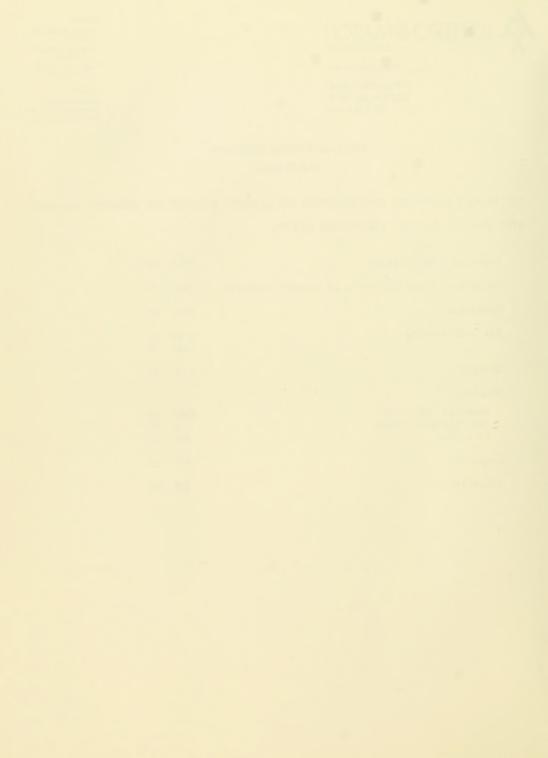
Associates

WILLIAM J HENNEY
RUDY A MARAMALDI PE
BRIAN M MCCORMAC+

# HYNES AUDITORIUM EXPANSION ELECTRICAL

PRELIMINARY ELECTRICAL LOAD BREAKDOWN FOR EXISTING BUILDING AND EXPANSION ADDITION
HVAC SYSTEM: ELECTRIC HEATING AND COOLING

Lighting & Receptacles	2804	KW
Exhibition Power exclusive of general lighting	3180	KW
Ventilation	3926	HP
Air Conditioning	4750 1000	KW HP
Heating	6250	KW
Plumbing:		
Domestic Hot Water	2000	KW
Miscellaneous Pumps Fire Pump	36 200	HP
rite rump	200	HP
Elevators	500	HP
Miscellaneous	100	KW





132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367

### ALFRED E LOTTERO PE PRESIDENT JOHN D DE VEUVE PE VICE PRESIDENT LOUIS A PERCOCO PE VICE PRESIDENT

Associates

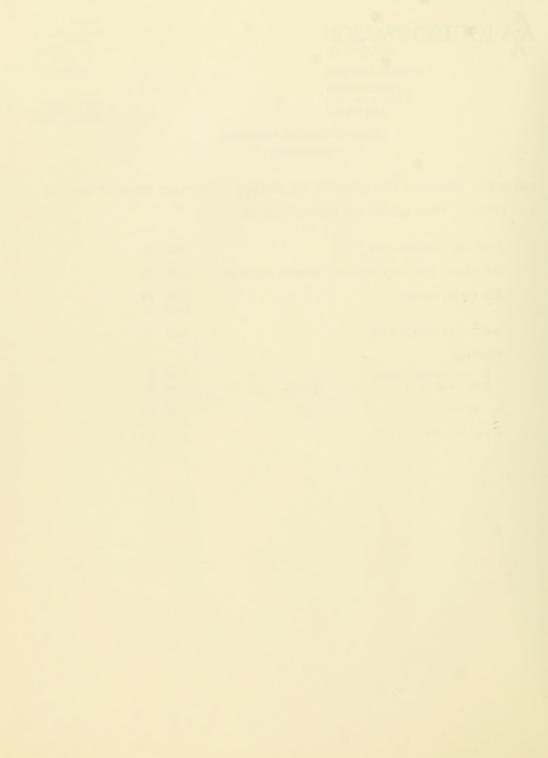
Principals

WILLIAM J HENNEY RUDY A MARAMALDI PE BRIAN M MCCORMACK

# HYNES AUDITORIUM EXPANSION ELECTRICAL

PRELIMINARY ELECTRICAL LOAD BREAKDOWN FOR EXISTING BUILDING AND EXPANSION ADDITION
HVAC SYSTEM: STEAM HEATING AND ELECTRIC COOLING

Lighting & Receptacles	2804	KW
Exhibition Power exclusive of general lighting	3180	KW
Air Conditioning	4750 1000	KW HP
Heating or Ventilating	3926	HP
Plumbing:		
Miscellaneous Pumps Fire Pump	36 200	HP HP
Elevators	500	HP
Miscellaneous	100	KW





132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367 Principals

ALFRED E LOTTERO PE
PRESIDENT

JOHN D DE VEUVE PE
VICE PRESIDENT

LOUIS A PERCOCO PE
VICE PRESIDENT

Associates

WILLIAM J HENNEY RUDY A MARAMALD PE BRIAN M MCCORMACK

# HYNES AUDITORIUM EXPANSION ELECTRICAL

PRELIMINARY ELECTRICAL LOAD BREAKDOWN FOR EXISTING BUILDING AND EXPANSION ADDITION

HVAC SYSTEM: STEAM HEATING AND COOLING

Lighting & Receptacles	2804	KW
Exhibition Power exclusive of general lighting	3180	KW
Air Conditioning	1000	HP
Heating or Ventilating	3926	HP
Plumbing:		
Miscellaneous Pumps	36	HP
Fire Pump	200	HP
Elevators	500	HP
Miscellaneous	100	KW





132 LINCOLN STREET BOSTON, MA 02111 (617) 423-7367 ALFRED E L'OTTERC PE PRESIDENT JOHN DI DE VEUVE PE VICE PRESIDENT LOUIS A PERCCICO PE VICE PRESIDENT

Associates

Principals

WILLIAM J HENNEY RUDY A MARAMALDI PE BPIAN M MOGORMACH

# HYNES AUDITORIUM EXPANSION ELECTRICAL

### PRELIMINARY ELECTRICAL EMERGENCY LOAD BREAKDOWN FOR EXPANSION ADDITION

Lighting	120	KW
Auxiliary Systems:		
Fire Alarm Telephone Security	25 10 20	KW KW KW
Plumbing:		
Fire Pump Jockey Pump Sewage Ejectors	200 5 10	HP HP HP
Smoke Exhaust Systems	150	HP
Elevators	100	HP
Miscellaneous	50	KW
Estimated size of Emergency Generator	750	KW

BACK BAY
B65M
1982

AUTHOR
Hynes Auditorium Expansion

TITLE
Final Rpt. (Vol.II-Part C)
BORROWER'S NAME
BORROWER'S NAME









